



Stainless Steel Helical Bevel Gearbox.

FKA



FKA Helical bevelgearbox

FKA series bevel gearboxes have been developed to achieve high torque, low energy use and less surface heat. The high efficiency of the drive reduces the energy consumption and the case hardened gears ensure a long lifetime and smooth running. Duplex stainless steel secondary shafts with PNS hardening contributes to a longer service life of the drive. Gearbox footprint, centerheight and shaftdiameters are interchangeable with common standards.

The design of Dertec gearboxes is round and smooth making the gearboxes extremely applicable in the food industry. The FKA bevel gearboxes offer high ratios up to 197,37 : 1, with a maximum output torque of 2700 Nm. Like all Dertec gearboxes, the FKA series is equipped with food grade lubrication.



Main Features

Made of high quality carefully electro polished Stainless Steel AISI 316 (mirror polished on request). The smooth design gives the gearbox a nice appearance, ready to suit all kinds of stainless steel machinery for the food industry.

Hardened shaft

All hollow shafts are produced in duplex stainless steel AISI 2205. The special PNS surface treatment ensures enough hardness to collaborate with our special high temperature resistant blue shaft seals. The PNS treatment increases the lifetime of shaft / seal cooperation and helps to reduce wear on the shaft surface.

The gearbox achieves a longer drip free operation compared to standard shaft / seal combinations made of AISI 304 with NBR or FKM.

The use of above combination offers all the positive characteristics of stainless steel and the surface hardness of a hardened shaft.

Blue shaft seals

Our high performance engineered shaft seals have a blue colour.

It is a well overthought feature for food industry applications.

It might be clear that the colour "blue" is a not existing organic colour.

In the context of food safety it is a common use to embed blue colours as these are very visible and easily to be recognised by vision scanning systems.

Foodgrade lubrication

All gearboxes are standard equipped with NSH H1 certified synthetic foodgrade lubrication.

On request it can be supplied with a halal, kosher or nut free certification.

Laser engraved tagplate

To avoid dirt traps under the commonly used motor identification tag plate, all our motors and gearboxes are being equipped with a laser engraved tag plate. Besides for the food safety this also prevents against possible loss of information because of taking away the tag plate or loosing the tag plate from the driveparts.

As a part of our standard procedure every drive is tested in our production facility in the Netherlands to ensure correct functioning.

General specifications

- Standard ratio's 3,98 : 1 to 197,37 : 1
- IEC motor adaption versions (AM)
- Integrated motor versions (B5T..)
- Standard hollow shafts 30, 35, 40, 50 & 60 mm
- Extra hygienic optional shaft covers. (open and closed version)
- Easy clean torque arm with built in elastic element to reduce mis alignment.
- High efficiency of 94%
- Optional output flanges available
- Stainless Steel AISI316
- Duplex stainless steel 2205 output shaft
- Interchangeable with euro sizes
- Designed and produced in the Netherlands



Product Characteristics

FKA 38	
Ratio's	From 3.98 : 1
	To 106.38 : 1
Standard shaft	30mm
Max. Torque	200 Nm
Max. Power	3.0 kW

FKA 48	
Ratio's	From 8.56 : 1
	To 131.87 : 1
Standard shaft	35 mm
Max. Torque	400 Nm
Max. Power	3.0 kW

FKA 68	
Ratio's	From 5.20 : 1
	To 144.79 : 1
Standard shaft	40 mm
Max. Torque	820 Nm
Max. Power	5.5 kW

FKA 78	
Ratio's	From 7.24 : 1
	To 192.18 : 1
Standard shaft	50 mm
Max. Torque	1550 Nm
Max. Power	7.5 kW

FKA 88	
Ratio's	From 7,21 : 1
	To 197.37 : 1
Standard shaft	60 mm
Max. Torque	2700 Nm
Max. Power	7.5 kW

Output Flanges		Easy Clean Open Cover		Easy Clean Closed Cover		Torque Arms	
FKA 38	SS 095 FL 160	FKA 38	SS 095 CO 030	FKA 38	SS 095 CC	FKA 38	SS 095 MS L130S
FKA 48	SS 115 FL 200	FKA 48	SS 115 CO 035	FKA 48	SS 115 CC	FKA 48	SS 095 MS L150
FKA 68	SS 130 FL 250	FKA 68	SS 130 CO 040	FKA 68	SS 130 CC	FKA 68	SS 115 MS L160S
FKA 78	SS 140 FL 250	FKA 78	SS 140 CO 050	FKA 78	SS 140 CC	FKA 78	SS 115 MS L200
FKA 78	SS 140 FL 300	FKA 88	SS 178 CO 060	FKA 88	SS 178 CC	FKA 88	SS 130 MS L200



Table of content

Table of Content

Table of content	5	General Dimensions	41
Project planning	7	General dimensions	42
Basic Parameters	8	Hollow shaft & Solid shaft	42
Power P		Hollow shaft	
Rotation speed n and gear ratio i		Solid shaft	
Torque M		Solid input shaft	43
Mass acceleration factor f_a	8	Shrink disk	43
Efficiency of gearboxes η	9	AM Flange dimensions	44
Service factor fs_{min} and $fs_{gearbox}$	9	Output flanges	44
Switching frequency		Open & Closed covers	45
Load classification		Torque arm	45
Service factor graph		Closed cover	45
Flowchart	12	Open cover	45
Elaborate method		Difference between B5T and B14a	46
Explanation of the flowchart		Extra information	47
Preferred method:		Mounting Positions	
Elaborate method:		Lubrication Quantity	
Example 1: Preferred method		Debreather Positions	
Example 2: Eleborate method		Terminal Box Positions	
Overhung and axial loads	18	Lubrication Type	
Rated bearing service life	18	Weight	
Preferred mounting for overhung loads	18		
Overhung load conversion for off-centre force applications			
The use of couplings			
Mounting of couplings			
Torque arm	21		
Mounting the torque arm			
Hollow shaft with key and shoulder			
Hollow shaft with key without shoulder			
Hollow shaft with a shrink disk			
Shrink disk specifications and installation			
Possible Geometrical Combinations	25		
FKA 38	26		
FKA 48	26		
FKA 68	27		
FKA 78	27		
FKA 88	28		
Gearbox Selection Tables	31		
0,12 - 0,18 kW	32		
0,18 - 0,25 kW	32		
0,25kW - 0,37 kW	33		
0,37 kW	33		
0,55 kW	34		
0,55 - 0,75 kW	34		
0,75 - 1,1 kW	35		
1,1 - 1,5 kW	35		
1,5 - 2,2 kW	36		
2,2 kW	36		
2,2 - 3 kW	37		
3 - 4 kW	37		
5,5 - 7,5 kW	38		
7,5 kW	38		

Project planning

Project Planning

Basic Parameters

Power P

The input power can be found in the "Gearbox Selection Tables", it represents the amount of kilowatts [kW] that can be safely transmitted into the gearbox.

$$P_1 = \frac{P_2}{\eta}$$

P_1	= Input power (kW)
P_2	= Output power (kW)
η	= Gearbox efficiency (%)

Rotation speed n and gear ratio i

The gear ratio can be calculated with the input and output speed

$$i = \frac{n_1}{n_2}$$

i	= Gear ratio
n_1	= Input speed in (rpm)
n_2	= Output speed in (rpm)

Torque M

The output torque can be calculated with the input power, the efficiency and the output speed.

$$M_2 = \frac{9550 \cdot P_1 \cdot \eta}{n_2}$$

$$M_{2\max} \geq M_2 \cdot fs_{\text{gearbox}}$$

M_2	= Output torque (Nm)
$M_{2\max}$	= Maximum output torque (Nm)
P_1	= Input power (kW)
n_2	= Output speed (rpm)
η	= Gearbox efficiency (%)
fs_{gearbox}	= Service factor

Mass acceleration factor f_a

The mass acceleration factor is calculated with all the external mass moments of inertia and the mass moment of inertia from the motor.

$$f_a = \frac{J_c}{J_m}$$

f_a	= Mass acceleration factor
J_c	= All external mass moments of inertia [kg m ²]
J_m	= Mass moment of inertia on the motor end [kg m ²]



If the mass acceleration factor $f_a \geq 10$, please contact us.

Efficiency of gearboxes η

The efficiency of gearboxes is mainly determined by the gear type, the gear ratio and the bearing friction. The efficiency of the gears at start-up and at sub-optimal operating speed is always lower than when the gears are running at the optimal operating speed. The gear shape of worm- and helical worm gearboxes causes more friction, thus a lower total efficiency. As a result of the higher friction, the temperature of worm gearboxes might also be higher than gearboxes with other gear types.

The efficiency of the different gear types can be found in the "**Possible Geometrical Combinations**".

For an approximate approach the following values can be used for the efficiency of gears at their (optimal) operational speed, beware these are generalized and can be different depending on the factors as discussed before.

For bevel-, helical- and parallel shaft gears the efficiency is in-between 94% (3-stage) and 96% (2-stage).

The efficiency of hypoid bevel gears is 90% (3-stage) and 92% (2-stage). For worm- and helical worm gears the efficiency depends on the gear ratio, incoming rotational speed and the temperature of the worm gearbox, the efficiency of the gears is between 40% and 90%.

To ensure the efficiency of the gears is optimal it is recommended but not limited to: Regularly change oil, use the optimal mounting position and use the gearbox at the optimal operating speed.

Choosing the right size gearbox for the application is recommended to achieve a better efficiency, at speeds below- and over the optimal operating speed the efficiency is lower than at optimal speeds and conditions.

Service factor fs_{min} and $fs_{gearbox}$

The service factor is a method to determine the effects of the driven machine or other application on the gearbox, with a sufficient level of accuracy for most applications. The minimal service factor (fs_{min}) for a machine can be determined using the "**Service factor graph**". This minimum service factor is only an approximation, for the service factor for each gearbox, see the "**Gearbox Selection Tables**".

 **The minimal service factor (fs_{min}) should always be lower than or equal to the actual service factor of the gearbox ($fs_{gearbox}$).**

$$fs_{min} \leq fs_{gearbox}$$

fs_{min} = Minimal determined service factor "**Service factor graph**"
 $fs_{gearbox}$ = Actual service factor for the gearbox "**Gearbox Selection Tables**"

 **The service factor for each gearbox ($fs_{gearbox}$) is the critical service factor, and should always be equal to or higher than the minimum service factor (fs_{min})!**

Switching frequency

The switching frequency determines how often an application switches per hour.

The switching consists of: **turning on/off, changing of speeds, changing of loads and braking**

Z = Switching frequency [1/h]

Project Planning

Load classification

There are three load classifications to be considered, they depend on the mass acceleration factor. The mass acceleration factor can be calculated, see "**Mass acceleration factor f_a** "

f_a = Mass acceleration factor

The load classifications are split in three groups with each examples of the common applications for each load classification.

A: Uniform load, a mass acceleration factor of $f_a \leq 0,3$

Examples of applications: Screw feeders for light materials, fans, assembly lines, conveyer belts for light materials, small mixers, light application elevators, cleaning machines, fillers, control machines.

B: Moderate shock load, mass acceleration of $f_a \leq 3$

Examples of applications: Winding devices, woodworking machine feeders, medium application elevators, balancers, medium mixers, conveyer belts for heavy materials, winches, sliding doors, fertilizer scrapers, packing machines, concrete mixers, crane mechanisms, milling cutters, folding machines, gear pumps.

C: Heavy shock load, mass acceleration factor of $f_a \leq 10$. Examples of applications: Mixers for heavy materials, shears, presses, centrifuges, rotating supports, winches and lifts for heavy materials, heavy application elevators, grinding lathes, stone mills, bucket elevators, drilling machines, hammer mills, cam presses, folding machines, turntables, tumbling barrels, vibrators, shredders.

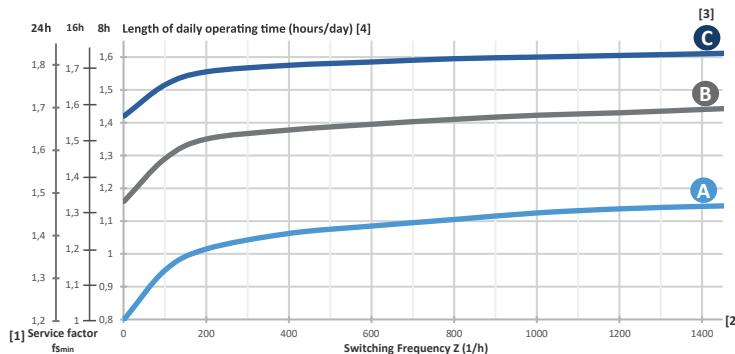
Service factor graph

The determined Minimum [1] service factor is based on [2] switching frequency, [3] load classification and [4] length of daily operating time.

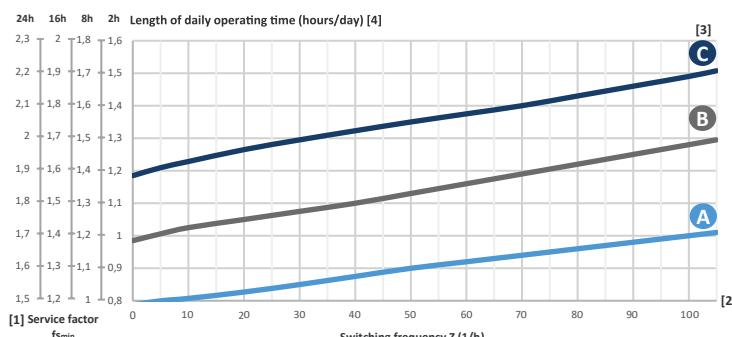


To get the expected service life from the gearbox, $f_{s\min} \leq f_s$ _{gearbox}
see the "Gearbox Selection Tables" for the gearbox service factor

Service factor for a high Switching frequency (Z), used for all gearboxes:



Service factor for low Switching frequency (Z), used mostly for worm- and helical worm gearboxes:



For worm gearboxes the ambient temperature has more influence on the service factor, the service factor should be adjusted as following:

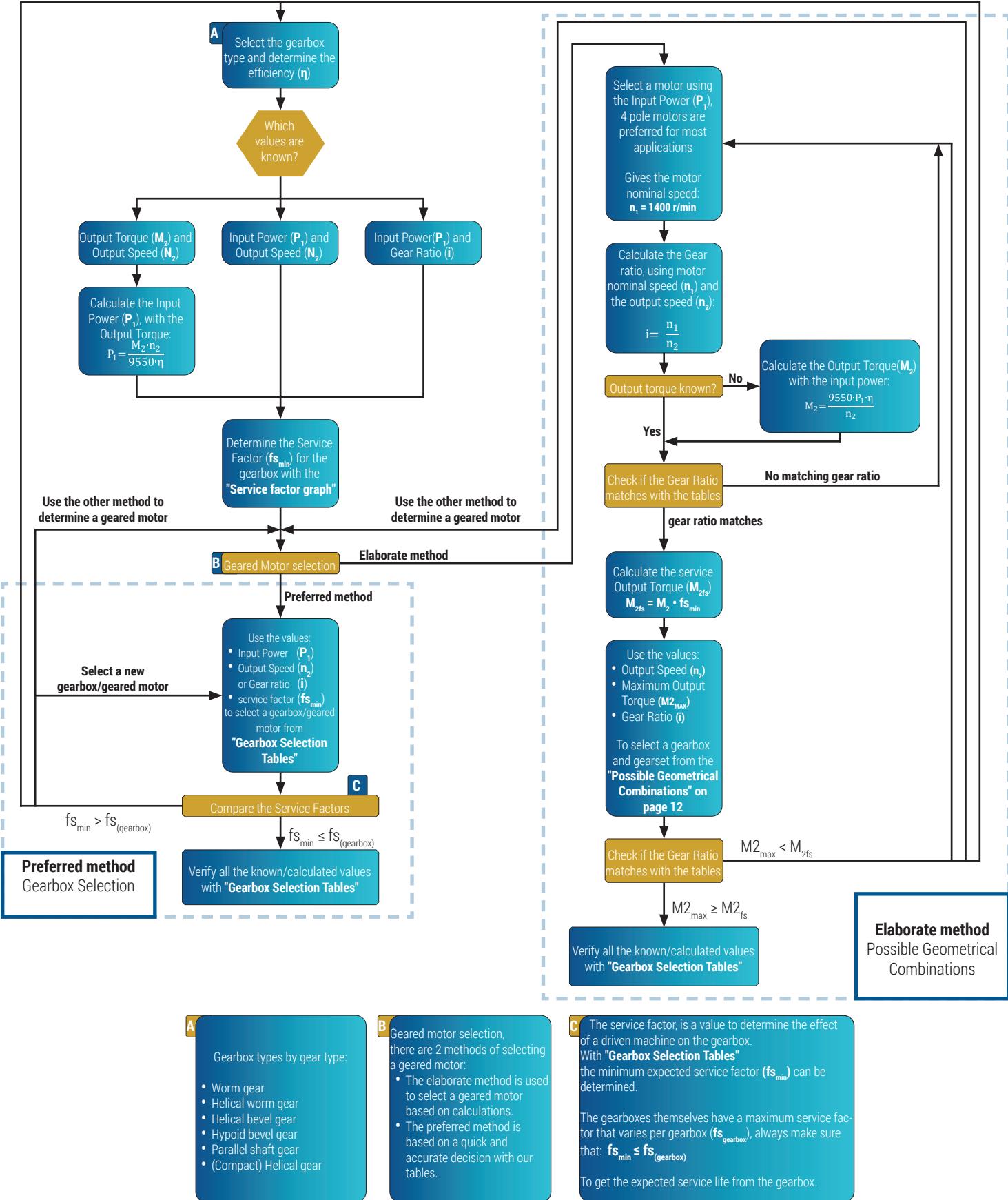
Ambient temperature:
=30~40°C, $f_s \cdot 1,1 \sim 1,2$
=40~50°C, $f_s \cdot 1,3 \sim 1,4$
=50~60°C, $f_s \cdot 1,5 \sim 1,6$

Project Planning

Select a different Gearbox type

Flowchart

Select a different Gearbox type



Explanation of the flowchart

Gearbox selection type

To select a gearbox the values for efficiency and the service factor are needed. These can be predicted by choosing the type of gearbox, "Possible Geometrical Combinations"

Which values are known?

There are three sets of values that can be known and which can be used to select the right gearbox and geared motor.

These three sets of values are:

- Output torque and speed
- Input power and speed
- Input power and gear ratio

For only knowing the output torque- and speed it is necessary to determine the input power with the following equation:

$$P_1 = \frac{M_2 \cdot n_2}{9550 \cdot \eta}$$

P_1	Input power [kW]
M_2	Output torque [Nm]
η	Gearbox efficiency [%]
n_2	Rotational speed [rpm]

Determine the service factor

Use the "Service factor graph" to determine the service factor.

Select a geared motor

There are two methods to select a gearbox and a geared motor:

The preferred method: This method is accurate and quick, this method only needs a basic calculation in when the input power is unknown.

The elaborate method: This method gives more insight and a more hands on approach in the selection process for a gearbox and geared motor.
There are a few calculations that have to be done in this method.



If both methods don't give the correct results it can be possible that the gearbox and or motor are not correct for this application!

Preferred method:

Use the "Gearbox Selection Tables"

Use the Input power, output speed or gear ratio and the service factor to select the gearbox/geared motor.



Note: that the output torque is sufficitated to your application

Check the service factor

Check if the determined service factor fs_{min} is smaller or equal to the service factor from the "Gearbox Selection Tables" $fs_{min} \leq fs_{gearbox}$.

If $fs_{min} > fs_{gearbox}$ a different gearbox/geared motor should be selected if that is not possible then it is advised to check the other gearbox types..

If $fs_{min} \leq fs_{gearbox}$ go to the next step and verify the results.

Verify the results

If the service factor fs_{min} and $fs_{gearbox}$ gives a valid result, verify the rest of the results with the tables from "Gearbox Selection Tables".

Elaborate method:

Select a motor

Select a motor from in the (**Motor documentation**).

4-pole motors are preferred for most applications. The given nominal motor speed of a 4-pole motor is $n_1=1400 \text{ rpm}$.

Calculate the gear ratio

If the gear ratio is known, the output speed n_2 needs to be calculated.

$$n_2 = \frac{n_1}{i}$$

With the nominal speed from the selected motor and known output speed the gear ratio can be calculated.

$$i = \frac{n_1}{n_2}$$

i = Gear ratio [-]

n₁ = Gearbox input speed [rpm] (equal to motor speed)

n₂ = Gearbox output speed [rpm]

Check if the output torque is known

If the output torque is known go to the next step.

If the output torque is unknown use the following calculation to determine the output torque:

$$P_1 = \frac{M_2 \cdot n_2}{9550 \cdot \eta}$$

P₁ = Input power [kW]

M₂ = Output torque [Nm]

η = Gearbox efficiency [%]

n₂ = Rotational speed [rpm]

Check the gear ratio

With the known or calculated gear ratio and the "**Possible Geometrical Combinations**", the gear ratio can be checked.

If the needed gear ratio is not in the list a different motor or gearbox should be selected.

Calculate the service output torque

With the determined service factor and the output torque, calculate the service output torque.

$$M_{2fs} = M_2 \cdot fs_{min}$$

M_{2fs} = Service output torque [Nm]

M₂ = Output torque [Nm]

fs_{min} = Service Factor

Use the Possible Geometrical Combinations tables

Use the Output speed, Service output torque and gear ratio to determine a gearbox and gearset with the tables from the "**Possible Geometrical Combinations**".

Check the maximum output torque

Check if the maximum output torque in these tables matches the calculated service output torque. If the maximum torque is lower than the calculated service torque: $M_{2max} < M_{2fs}$ it is advised to select a different motor or gearbox.

If $M_{2max} \geq M_{2fs}$ go to the next step and verify the results.

Verify the results

If the maximum output torque matches the tables and gives a valid result, then verify the values from the tables with the calculated values and make a selection for the gearbox/geared motor.

Example 1: Preferred method

Known parameters:

M_2	Nominal output torque [Nm]	= 110 Nm
n_2	Rotational speed [rpm]	= 29 rpm

Moderate shock load, operational **16 hours a day**, Switching frequency of **200 times per hour**.

Gearbox selection type

A hypoid bevel gearbox is selected. The estimated efficiency $\eta \approx 90\% \text{ to } 94\%$. For a more accurate efficiency look it up in the "Possible Geometrical Combinations".

When in doubt use the lowest estimated efficiency.

Which values are known?

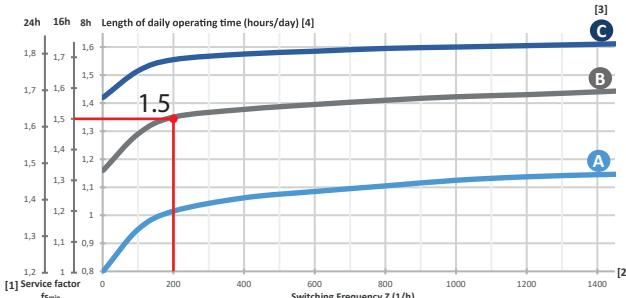
- Output torque- and speed
- Input power- and speed
- Input power and gear ratio

$$\begin{aligned} M_2 &= 110 \text{ Nm} \\ n_2 &= 29 \text{ rpm} \end{aligned}$$

Looking up the output speed and output torque in the "Possible Geometrical Combinations" on page 15 tables gives an efficiency of: $\eta \approx 92\%$. With the output torque- and speed it is necessary to determine the input power with the following equation:

$$P_1 = \frac{M_2 \cdot n_2}{9550 \cdot \eta} = \frac{110 \cdot 29}{9550 \cdot 0,92} = 0,363 \text{ kW}$$

Determine the safety factor



Select the 'Elaborate method' or the 'Preferred method'

Preferred method is chosen.

P_{1n} [kW]	n_2 min ⁻¹	M_{2n} [Nm]	i	F_{r2} [N]	fs		
0.37	23	140	60.50	3430	1.40		
	29	113	48.71	3190	1.80		
	36	91	39.29	2970	2.00		
	46	70	30.31	2720	2.80	FK38B IEC71	712-4 B14a
	57	57	24.44	2530	3.20		
	69	47	20.25	2380	3.20		
	95	34	14.67	2130	3.20		

Check the service factor

$$\begin{aligned} fs_{min} &= 1,5 \\ fs_{(gearbox)} &= 1,8 \end{aligned}$$

Check if the following is true

$$fs_{min} \leq fs_{(gearbox)}$$

Yes, because $1,5 < 1,8$

Verify the results

Needed Torque: **110 Nm**, available torque in selected gearbox: **113 Nm**

Needed output speed: **29 rpm**, available output speed in selected gearbox: **29 rpm**

Calculated Input power: **0,363 kW**, available input power in selected gearbox: **0,37 kW**

Service factor: $fs_{min} \leq fs_{(gearbox)} = 1,5 < 1,8$

So the choice of gearbox/geared motor is: **FK38B IEC71 / 712-4 B14a**.

⚠ It is recommended to select a gearbox or geared motor that fits the application. Choosing a gearbox or geared motor that is too light or too heavy can cause damage (to the machine) and shorten the expected service life of the gearbox/geared motor!

Project Planning

Example 2: Eleborate method

This example uses a different gearbox type but is generally applicable

Known parameters:

P₁ Input power [kW] = **0.55kW** i gear ratio = **30:1**
 Heavy shock load, operational **24 hours a day**, switching frequency of **800 times per hour**.

Gearbox selection type

A hypoid bevel gearbox is selected. The estimated efficiency $\eta \approx 90\% \text{ to } 94\%$. For a more accurate efficiency look it up in the "Possible Geometrical Combinations"

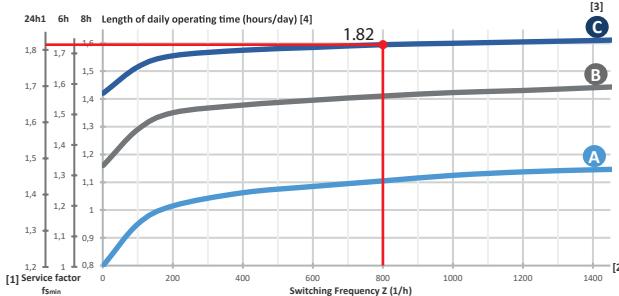
When in doubt use the lowest estimated efficiency.

Which values are known?

- Output torque and speed
 - Input power and speed
 - Input power and gear ratio
- P₁ = **0.55 kW**
 i = **30:1**

Looking up the output speed and output torque in the "Possible Geometrical Combinations" tables gives an efficiency of: $\eta \approx 94\%$

Determine the safety factor



Select the elaborate or the Simple method

Elaborate method is chosen

Select a motor

Check the "Possible Geometrical Combinations", which motor is preferred. In this example an IEC80 B14a motor is preferred.



The choice of motor is based on a 4-pole motor, which means an input speed of 1400 rpm.

However it is possible to choose from a wide range of motors.

Calculate the output speed

$$i = 30:1$$

$$n_1 = 1400 \text{ rpm}$$

$$i = \frac{n_1}{n_2} \rightarrow n_2 = \frac{n_1}{i} \rightarrow \frac{1400 \text{ rpm}}{30} = 46,67 \text{ rpm}$$

Check of the output torque is known

The output torque is not known yet, so it needs to be calculated with the known values.

$$M = \frac{9550 \cdot P \cdot \eta}{2} = \frac{9550 \cdot 0,55 \cdot 0,90}{46,67 \text{ rpm}} = 101,3 \text{ Nm}$$

Check the gear ratio

To check the gear ratio, look in the "Possible Geometrical Combinations" tables for the preferred gearbox. As seen below, the gear ratio and output speed match with this gearbox. The preferred motor is also possible with this gearbox type.

FK 28 B

Maximum torque = 130 Nm @ N1 = 1400 rpm

n ₂ [min ⁻¹]	M _{2max} [Nm]	F _{r2} [N]	i	η%	IEC 63 B5	IEC 71 B14a	IEC 80 B14a	IEC 90 B14a
35	130	2610	40	40.09	94	✓	✓	✓
48	130	2350	30	29.33	94	✓	✓	✓
59	130	2200	25	24.07	94	✓	✓	✓

Calculate the service output torque

Use the determined service factor and the calculated output torque.

$$M_{2fs} = M_2 \cdot fs_{min} \rightarrow 101,3 \text{ Nm} \cdot 1,82 = 184,37 \text{ Nm}$$

Use the Possible Geometrical Combinations tables

FK 28 B

Maximum torque = 130 Nm @ $N1 = 1400 \text{ rpm}$

n_2 [Min ⁻¹]	M_{2max} [Nm]	F_{r2} [N]	i	$\eta\%$	IEC 63 B5	IEC 71 B14a	IEC 80 B14a	IEC 90 B14a
35	130	2610	40	40.09	94	✓	✓	✓
48	130	2350	30	29.33	94	✓	✓	✓
59	130	2200	25	24.07	94	✓	✓	✓

Check the maximum output torque

With the known values and the selected gearbox, we can determine that the following values apply:

$$n_2 = 48 \text{ rpm} \approx 46.67 \text{ rpm [calculated]}$$

$$i = 30 = 30 \text{ [known]}$$

$$M_{2fs} = 101,3 \text{ Nm} \text{ [calculated]}$$

So the determined gearbox has enough output torque for the application 130 Nm, but when we look at the service output torque, it is not recommended to choose this gearbox with this service factor and service output torque.

$$M_{2fs} = 184,37 \text{ Nm} \text{ [calculated]}$$

$$M_{2max} < M_{2fs} \rightarrow 130 \text{ Nm} < 184,37 \text{ Nm}$$


[It is recommended to choose another gearbox](#), the easiest way to do this is to look for a bigger gearbox within the same gearbox type.

Selecting a new gearbox

It is recommended to match the calculated results as before, but look for a higher maximum torque. Try to select a maximum torque that still matches the application, it is not recommended to select a gearbox with more maximum torque than the application needs.

FK 38 B

Maximum torque = 200 Nm @ $N1 = 1400 \text{ rpm}$

n_2 [Min ⁻¹]	M_{2max} [Nm]	F_{r2} [N]	i	$\eta\%$	IEC 63 B5	IEC 71 B14a	IEC 80 B14a	IEC 90 B14a
36	200	2970	40	39.29	94	✓	✓	✓
47	200	2720	30	30.31	94	✓	✓	✓
58	200	25030	25	24.44	94	✓	✓	✓

Verify the results

With the table for the FK38B gearbox, we can determine the following.

$$n_2 = 47 \text{ rpm} \approx 46.67 \text{ rpm [calculated]}$$

$$i = 30 = 30 = \text{[known]}$$

$$M_2 = 101,3 \text{ Nm} \text{ [calculated]}$$

$$M_{2fs} = 184,37 \text{ Nm} \text{ [calculated]}$$

Check if the maximum output torque is higher than the service output torque.

$$M_{2max} > M_{2fs} \rightarrow 200 \text{ Nm} > 184,37 \text{ Nm}$$

So this gearbox can be used for the application, because the service output torque is lower than the maximum output torque.

The recommended gearbox with motor is:

For a gearbox, a **FK38B** with a true gear ratio of **30,31** and for a motor, the **IEC80 B14a** is possible.



It is recommended to select a gearbox or geared motor that fits the application. Choosing a gearbox or geared motor that is too light or too heavy can cause damage (to the machine) and shorten the expected service life of the gearbox/geared motor

Project Planning

Overhung and axial loads

Determining overhung loads

Each transmission element has a transmission element factor f_z , this factor is different for each element.

In order to properly use transmission elements, always make sure that they are aligned properly on the shaft of the gearbox and or the shaft of the machine or other application. It is important to check that the transmission element is mounted properly before use, the element might cause problems in dynamic situations if this isn't checked

$$F_r = \frac{M \cdot 2000}{d_0} \cdot f_z$$

F_r = overhung load [N]
M = Torque [Nm]
d₀ = Mean diameter of the mounted element [mm]
F_z = Element factor [see table above]

Transmission elements	Transmission elements Factor F _z	Comments
Gears	1.00	≥ 17 Teeth
	1.15	< 17 Teeth
Chain sprockets	1.00	≥ 20 Teeth
	1.25	< 20 Teeth
Narrow V-belt Pulleys	1.40	< 13 Teeth
	1.75	Influence of the tensile force
Flat Belt Pulleys	2.50	Influence of the tensile force
Toothed Belt Pulleys	2.50	Influence of the tensile force

Rated bearing service life

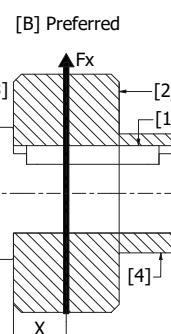
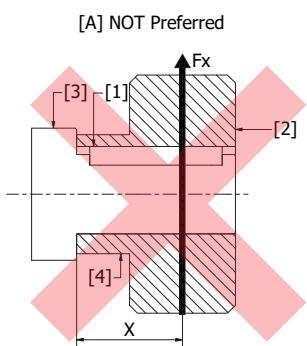
The rated bearing service life L_{10h} (in hours, according to **ISO 281**) is used to calculate the estimated bearing life in hours. For special operating conditions the modified service life should be used.

$$L_{10h} = \frac{10^6}{60 \cdot n_2} \cdot \left(\frac{C}{F_r} \right)$$

L_{10h} = Rated service life [hour]
C = Basic dynamic load rating, bearing [kN]
F_r = Equivalent dynamic load, bearing [kN]
p = Exponent for the life equation, p=3 for ball bearings, p=10/3 for roller bearings
n₂ = Gearbox output speed [rpm]

Preferred mounting for overhung loads

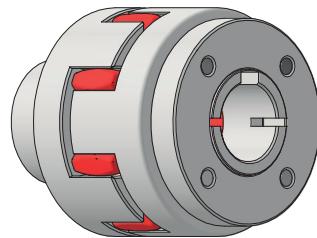
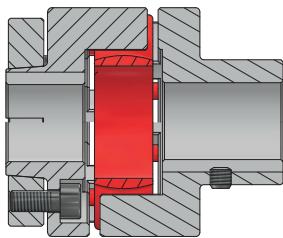
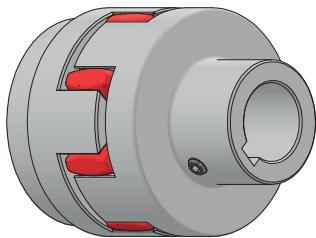
The preferred way of mounting the overhung load for sprockets, gears and other transmissions is with the hub **[4]** at the end of the shaft **[3]** and the sprocket/gear **[2]** against the shoulder, see **[B]** in the figure below. This method ensures a better load distribution on the end of the shaft.



nr.	Part Name
[1]	Key
[2]	Sprocket / Gear
[3]	Solid shaft
[4]	Hub
[Fx]	Radial Force on the Sprocket / Gear
[X]	Distance to center of mass and force

Project Planning

The use of couplings



Example of a flexible coupling

Couplings are usually needed when a gearbox is rigidly mounted to a machine or other application. A coupling offers some room for misalignment that may be present or develop during use of the gearbox.

⚠ Not all misalignments can be statically determined, some may develop during dynamic processes are only present during use of the gearbox

Couplings give room for these misalignments and ensure the service life of the bearings inside of the gearbox, by offering a bit more room for error when there are misalignments.

There are different types of couplings that can be used in such applications, one example is a flexible coupling, *see: example of a flexible coupling*. Flexible couplings often have three parts, one for the shaft of the machine or application, one for the shaft of the gearbox and a part that gives flexibility. The flexible part is often made of rubber or another kind of polymer.

⚠ Note: A coupling slightly increases the temperature of the shafts, due to friction and slightly decreases the efficiency of the gearbox.

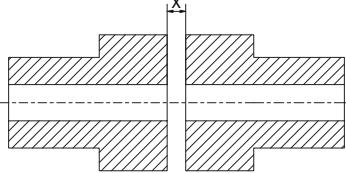
Mounting of couplings

To properly mount the couplings and prevent excessive wear on the gearbox, it is necessary to mount the couplings correctly. To mount a coupling properly please pay attention to the following types of misalignment.

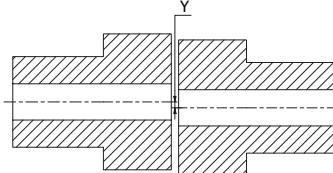
⚠ Note: The amount of allowable misalignment is often specified in the coupling datasheet, from the coupling manufacturer

⚠ Never mount couplings onto the shaft by hitting them with a hammer, this can cause damage to the gearbox bearings and can reduce the gearbox service life

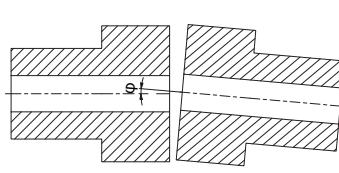
[A] Axial misalignment / Clearance



[B] Offset misalignment



[C] Angular misalignment



[A] Horizontal misalignment/Clearance:

Make sure that the horizontal misalignment/clearance [X] does not exceed the minimum and maximum clearance. This value is dependant on the type of coupling, material of the coupling and bore/shaft diameter and length. $X_{min} \leq X \leq X_{max}$, where $X_{min} > 0$.

⚠ Note: For the allowable clearance see the coupling manufacturers data sheet.

[B] Axial misalignment:

Make sure that the axial misalignment [Y] is as close to 0 as possible, in general axial misalignment will cause wear when the misalignment is too big.

[C] Angular misalignment:

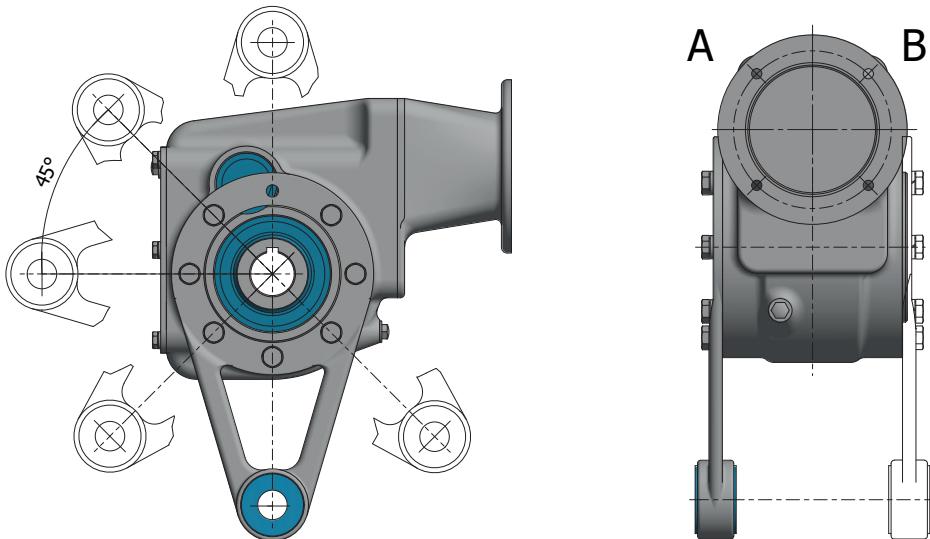
Make sure the angular misalignment [ϕ] is as close to 0 (degrees) as possible, excessive angular misalignment will cause damage.

⚠ Couplings allow small misalignments, but excessive misalignment and couplings that aren't mounted properly can still cause damage to the gearbox and or machine or other applications.

Torque arm

A torque arm is an attachment for a gearbox that prevents the gearbox from spinning with the driven shaft. When a gearbox is mounted directly on the output shaft without any external support it is always necessary to use a torque arm.

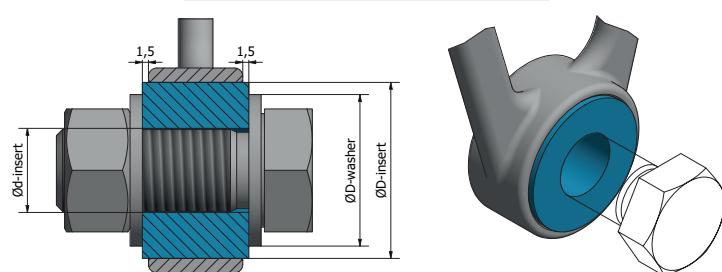
Depending on the gearbox type and size, torque arms can be mounted in a multitude of different positions on the output sides of the gearbox, see the figure below for an example of the different positions.



When mounting the torque arm pay attention to the following:

- A torque arm is used to prevent the gearbox from turning with the driven shaft, the torque arm does not prevent movement.
- It is important that the gearbox is allowed some movement when using a torque arm, to ensure that the gearbox bearings don't wear excessively.
- Make sure that the gearbox has enough clearance around it, so it is not in direct contact with the surroundings.
- It is always recommended to mount the torque arm on the gearbox side closest to the machine, this lowers the probability and the effect of misalignment.
- Avoid mounting the torque arm to a separate frame, this could cause misalignment. Mounting to the machine/application is always preferred.
- Always make sure the torque arm is properly mounted to the gearbox, and all available mounting holes are used.
- When using a torque arm, pay attention when mounting the torque arm to a "fixed" position. The torque arm should have enough room to move freely and should not be mounted too tight.
- When attaching the torque arm to a "fixed" position with a bolt, make sure that the bolt is hand tightened and that the rubber insert is not tightened too firm.
- Make sure when using a bolt to hold the torque arm in place, that the washer is smaller than the rubber insert (see figure below).
- If the rubber insert moves out of place, the alignment is not done properly. This does not mean that the torque arm is not tightened properly.

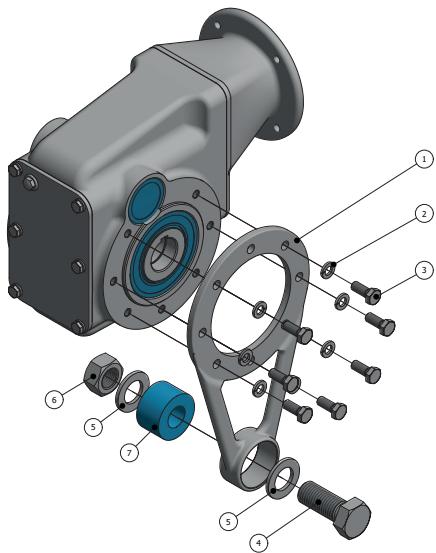
	ϕ D-ring [mm]	ϕ D-insert [mm]	ϕ d-insert
MSB 2510	<25	25	10
MSB 4320	<43	43	20



Project Planning

Mounting the torque arm

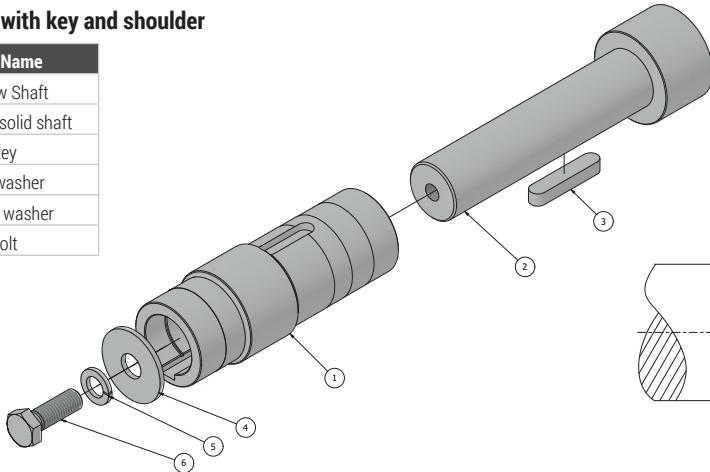
To mount the torque arm, mount the [1] torque arm to the gearbox and bolt it down with [2] spring washer and [3] bolts of the right size. Attach the holding [4] bolt with a [5] washer, through the hole of the [7] rubber insert. Add another [5] washer on the opposite side of the [7] rubber insert and attach the [6] nut hand tight to the holding [4] bolt.



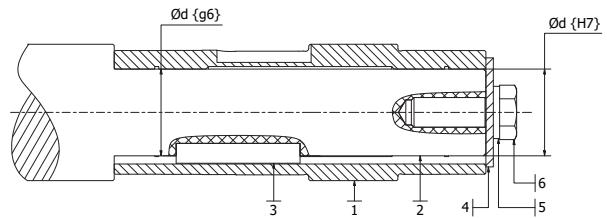
nr.	Part Name
1	Torque arm
2	Spring washer
3	Bolt
4	Bolt
5	Washer
6	Nut
7	Rubber insert

Hollow shaft with key and shoulder

nr.	Part Name
1	Hollow Shaft
2	Machine solid shaft
3	Key
4	Flat washer
5	Spring washer
6	Bolt

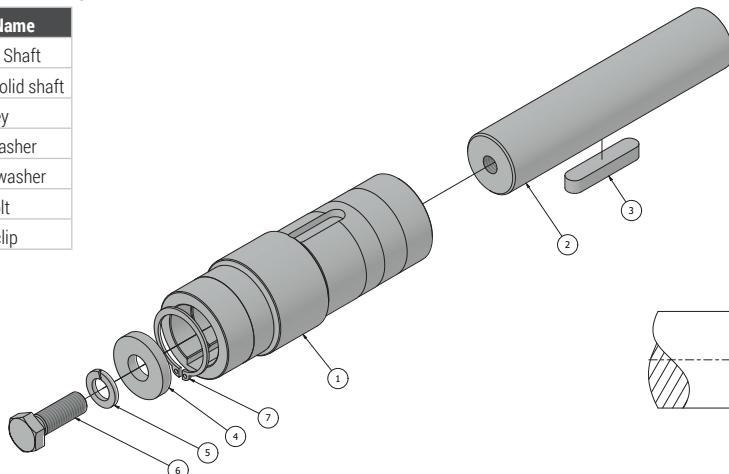


A machine shaft with a key and shoulder is usually held in place with a bolt, a lock washer and a flat washer on the outside of the hollow shaft.

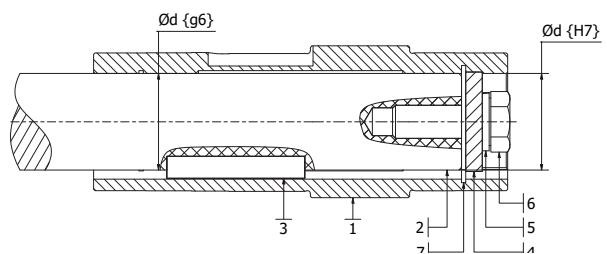


Hollow shaft with key without shoulder

nr.	Part Name
1	Hollow Shaft
2	Machine solid shaft
3	Key
4	Flat washer
5	Spring washer
6	Bolt
7	Circlip



A machine shaft with a key and without shoulder is usually held in place with a bolt, lock washer, a thick flat washer and a circlip on the inside of the hollow shaft.

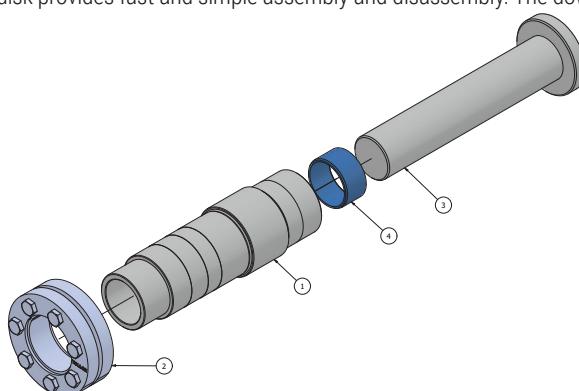


Hollow shaft with a shrink disk

For some applications a shrink disk is preferred, this is a disk that is installed on a longer hollow shaft, which clamps down onto its shaft. This friction holds the machine shaft inside the hollow shaft in place. Because of the friction fit, the machine shaft does not need to have a key in it.

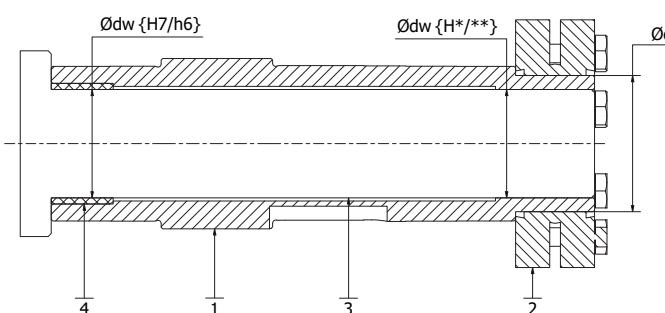
The benefit of a shrink disk is that it provides a way for easy removal of the shaft. Because it is a friction fit, no contact corrosion forms between the shafts. Also it provides an extra fail safe when the machine locks up. The gearbox will not be damaged because the shrink disk will slip when too much torque is applied. A shrink disk provides fast and simple assembly and disassembly. The downside to a shrink disk is that it takes up more space.

nr.	Part Name
1	Hollow Shaft SD
2	Shrinkdisk
3	Machine solid shaft
4	Spacer tube



Shrink disk specifications and installation

The measurements for the machine shaft diameter and the tolerances are shown in the table below. Here the amount of screws and screw type with the tightening torque are also shown.

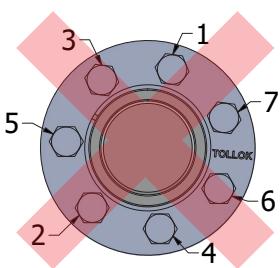


Ød [mm]	Ødw size [mm]	Ødw {H*/**} tolerance	Tightening screws [N° X Type]	Tightening torque [Nm]
14	11-12	H6/j6	4 x M5	
16	13-14		5 x M5	
24	19-21		6 x M5	4
30	24-26		7 x M5	
>30	24-26	H6/h6	5 x M6	
36	28-31		7 x M6	
44	32-36		8 x M6	12
50	38-42		10 x M6	
>50	38-42	H6/g6		
55	42-48			
62	48-52			
68	50-55			
75	55-65	H7/g9		
80	60-75		7 x M8	30
>80	60-75			

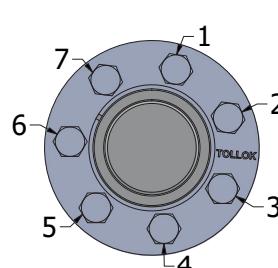
In order to ensure the shrinkdisk is used correctly the following has to be taken into account:

- When the shrink disk is untightened, make sure the screws don't get loosened all the way, this could cause them to fall out.
- When tightening the shrink disk do this in the correct order according to [B] with the right amount of torque as shown in the table. If tightening is not done properly situation [E] unequally tightened can occur.

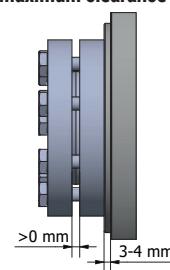
[A] Incorrect tightening order



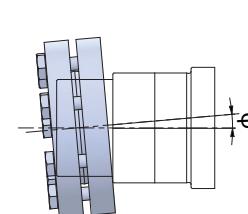
[B] Correct tightening order



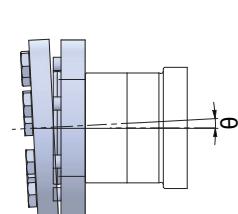
[C] Minimum and maximum clearance



[D] Angular misalignment



[E] Unequally tightened



Possible Geometrical Combinations

Possible Geometrical Combinations

FKA 88

Maximum Torque = 2700 Nm @ N1 = 1400 r/min

n ₂ [Min ⁻¹]	M _{2max} [Nm]	Fr ₂ [N]	i	η%						
					AM	B5T1	AM	B5T1	AM	B5T1
	IEC80	IEC90	IEC100	IEC112	IEC132					
7,1	2700	27300	197,37	94%		V				
8	2700	27300	174,19	94%		V	V			
8,5	2700	27300	164,34	94%		V	V			
9,5	2700	27300	147,32	94%		V	V	V		
11	2700	27300	126,91	94%		V	V	V	V	
12	2700	27300	115,82	94%		V	V	V	V	
14	2700	27300	102,71	94%		V	V	V	V	V
16	2700	27300	86,34	94%		V	V	V	V	V
18	2700	27300	79,34	94%		V	V	V	V	V
20	2700	27300	70,46	94%		V	V	V	V	V
22	2700	26200	63,0	94%		V	V	V	V	V
25	2700	25000	56,64	94%		V	V	V	V	V
28	2700	23500	49,16	94%			V	V	V	V
32	2600	22800	44,02	94%				V	V	V
38	2500	21400	36,52	94%				V	V	V
45	2700	19200	31,39	94%		V	V	V	V	V
50	2600	18500	27,88	94%		V	V	V	V	V
56	2500	18000	24,92	94%			V	V	V	V
62	2300	17900	22,41	94%			V	V	V	V
72	2300	16800	19,45	94%			V	V	V	V
80	2200	16300	17,42	94%				V	V	V
88	1800	16000	16,0	94%		V	V	V	V	V
97	2100	15300	14,45	94%				V	V	V
111	2000	14800	12,56	94%						V
125	1500	14900	11,17	94%			V	V	V	V
140	1500	14200	10,0	94%				V	V	V
169	1400	13500	8,29	94%				V	V	V
194	1300	13200	7,21	94%						V





Possible Geometrical Combinations

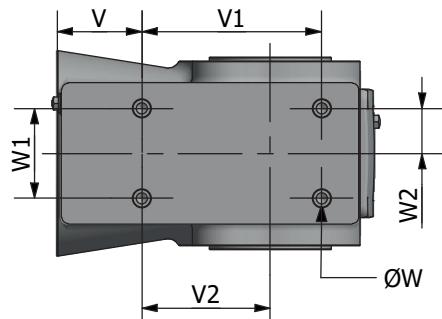
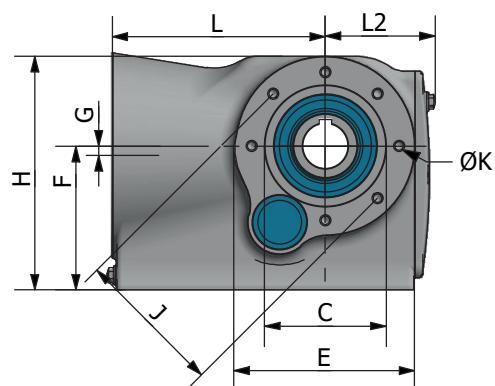
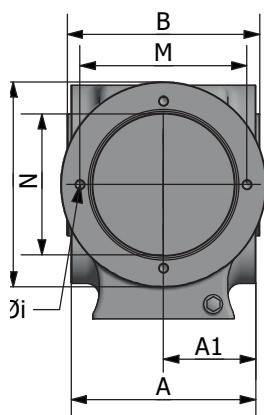
Gearbox Selection Tables

P_{1n}	= Rated Motor Power [kW]	M_{2max}	= Maximum permissible output torque [Nm]	$\eta\%$	= Transmission Efficiency %
n_2	= Output Speed [Min ⁻¹]	F_{t^2}	= Permitted Overhung Load Output Side [N]	f_s	= Service Factor
M_{2n}	= Rated Output torque [Nm]	i	= Gear unit Ratio		

General Dimensions

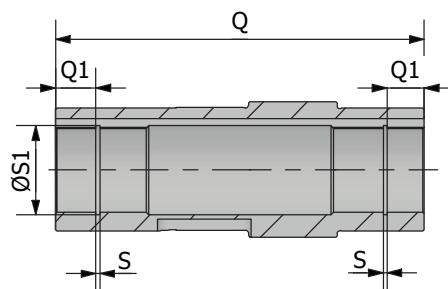
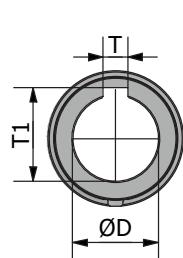
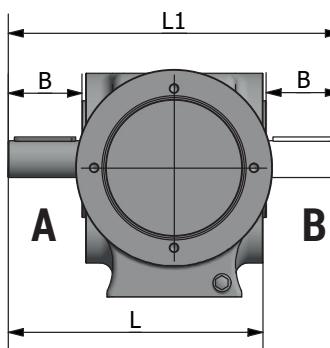
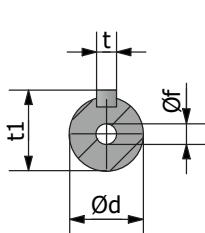
General Dimensions

General dimensions



Gearbox	A	A1	B	C	E	F	G	H	Øi	J	ØK	L	L2	M	N	P	V	V1	V2	ØW	W1	W2
FKA 38 B5T1	115	57,5	121	80	110	100	8,5	161,5	M6	95	M8	139	76	100	80	120	57	117	82	M10	60	30
FKA 48 B5T2	144	72	150	95	140	112	7,2	185	M8	115	M8	166	86	130	110	160	66	140	100	M10	70	35
FKA 68 B5T2	173	86,5	179	110	160	140	20	226	M8	130	M10	179	110,5	130	110	160	69	152	110	M12	88	44
FKA 78 B5T3	202	101	208	118	170	180	31,4	280,5	M12	140	M12	202	111,5	165	130	200	80	170	122	M16	102	51
FKA 88 B5T4	232	116	240	150	215	212	26,1	342	M12	178	M16	257	136,5	215	180	250	97	225	160	M16	118	59

Hollow shaft & Solid shaft



Hollow shaft

Gearbox	ØD [H7/h6]	T	T1	Q	Q1	S	S1
FKA 38	30	8	33,3	120	13,7	1,3	31,4
FKA 48	35	10	38,3	150	16,7	1,6	37
FKA 68	40	12	43,3	179	22,5	1,85	43
FKA 78	50	14	53,8	208	26	2,65	53
FKA 88	60 [H8/h6]	18	64,4	240	27,7	2,3	63,2

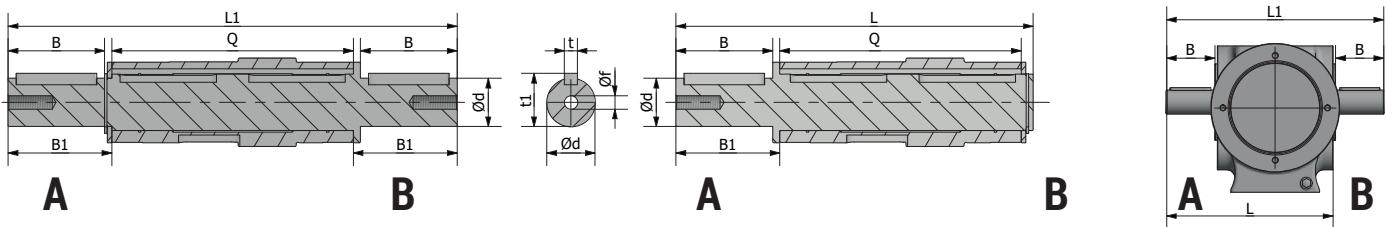
Different solid shaft dimensions possible on request

Solid shaft

Gearbox	Ød [g6]	Øf	t	t1	L	L1	B
FKA 38	25	M10	8	28	170	220	50
FKA 48	30	M10	8	33	210	270	60
FKA 68	40	M16	12	43	159	339	80
FKA 78	50	M16	14	53,5	308	408	100
FKA 88	60	M20	18	64	460	480	120

Different solid shaft dimensions possible on request

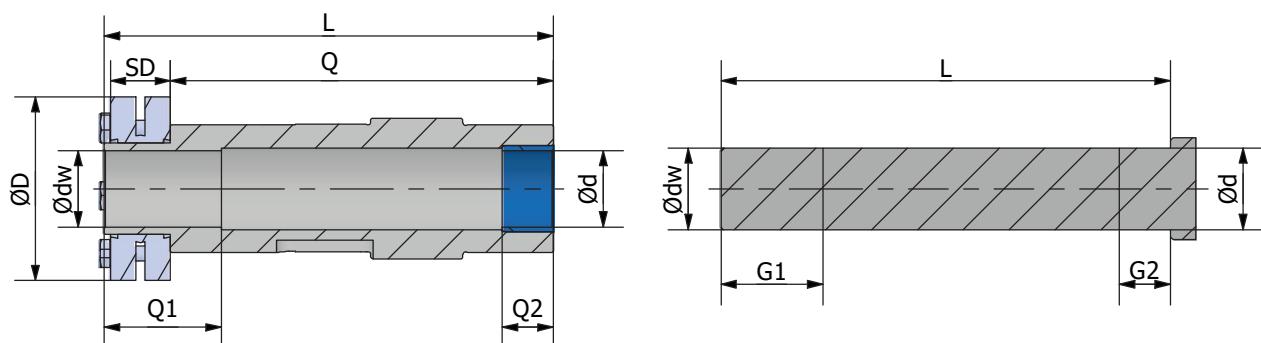
Solid input shaft



Gearbox	$\text{Ød}[h6]$	B	B1	Q	L	L1	Øf	t	t1
FKA 38	25	50	53,5	120	182	227	M10	8	28
FKA 48	30	60	64,5	150	222	279	M10	8	33
FKA 68	40	80	84,5	179	274	384	M16	12	43

Different solid input shaft dimensions possible on request

Shrink disk



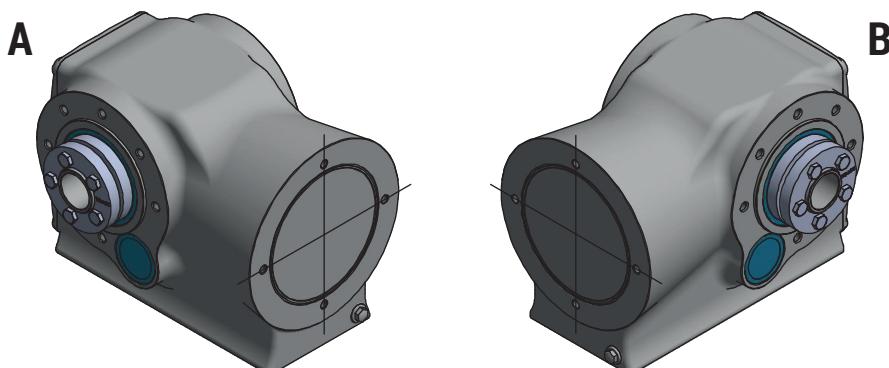
Gearbox	$\text{Ød}[H7/h6]$	$\text{Ødw}[H6/*]$	ØD	L	SD	Q	Q1	Q2	G1	G2	N° x Type	Ms [Nm]	Mt [Nm]
FKA 38	30	30 [*h6]	72	143,5	23,5	120	31	20	36	25	5 x M6	12	570
FKA 48	35	35 [*h6]	80	175,5	25,5	150	32	20	37	25	7 x M6	12	780
FKA 68	40	40 [*h6]	90	206,5	27,5	179	38	20	43	25	8 x M6	12	1160
FKA 78	50	50 [*g6]	110	238,5	30,5	208	36	30	41	35	10 x M6	12	2200
FKA 88	60	60 [*g6]	115	270,5	30,5	240	41	40	46	45	10 x M6	12	3150

Different shrinkdisk dimensions possible on request

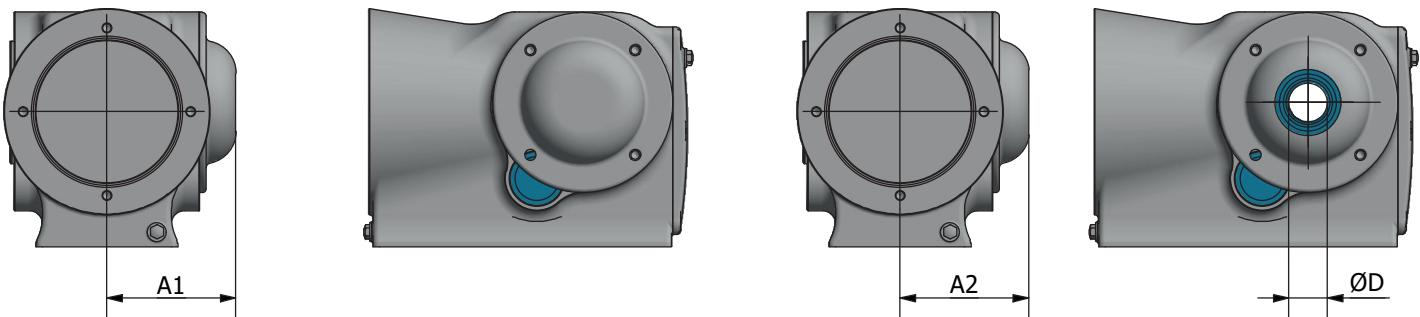
From 18 mm to 30 mm H6/j6

From 30 mm to 50 mm H6/h6

* depends on the shaft diameter



Open & Closed covers



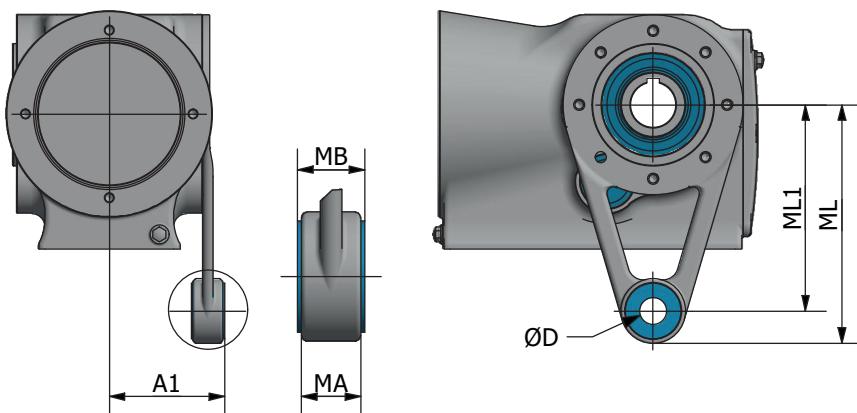
Closed cover

Gearbox	Closed cover	A1
FKA 38	SS 095 CC	83,5
FKA 48	SS 115 CC	100
FKA 68	SS 130 CC	114,5
FKA 78	SS 140 CC	130
FKA 88	SS 178 CC	151

Open cover

Gearbox	Open cover	A2	ØD
FKA 38	SS 095 CO30	79,5	30
FKA 48	SS 115 CO35	100	35
FKA 68	SS 130 CO40	114,5	40
FKA 78	SS 140 CO50	130	50
FKA 88	SS 178 CO60	151	60

Torque arm

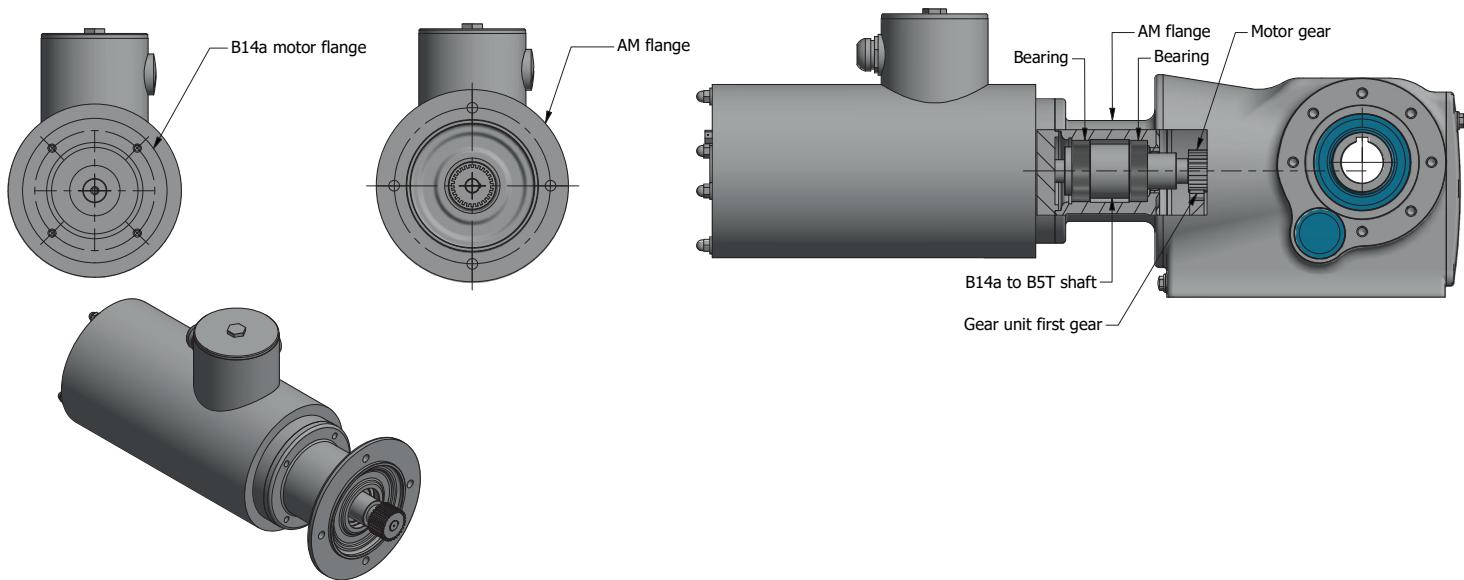


Gearbox	Torque arm	A1	MA	MB	ØD	ML	ML1
FKA 38	SS 095 MS L130S	69,3	12	15	10,5	146	130
	SS 095 MS L150	69,3	12	15	10,5	166	150
FKA 48	SS 115 MS L160S	89,3	23	26	20,5	185	160
	SS 115 MS L200	89,3	23	26	20,5	225	200
FKA 68	SS 130 MS L200	105	23	26	20,5	225	200
FKA 78	SS 140 MS L250	124	23	26	20,5	285	250
FKA 88	SS 178 MS L300	139	23	26	20,5	335	300

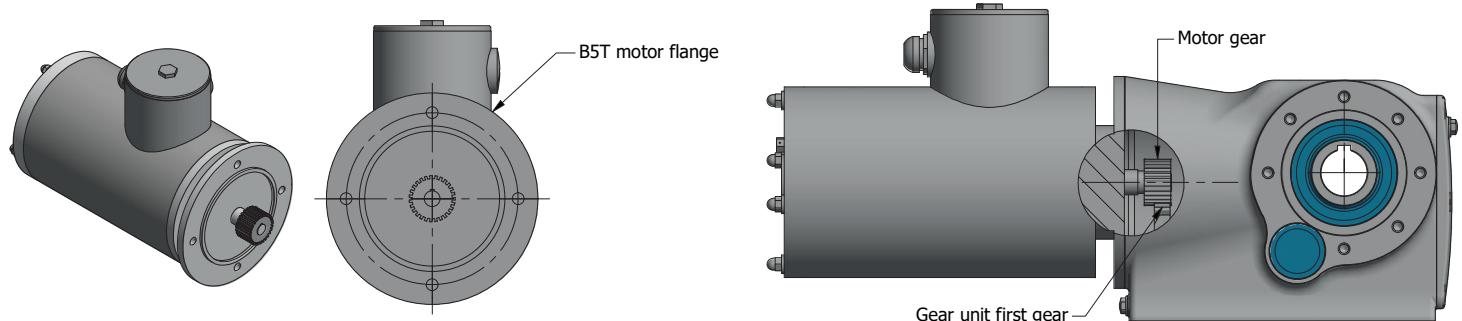
General Dimensions

Difference between B5T and B14a

B14a motor with AM - flange

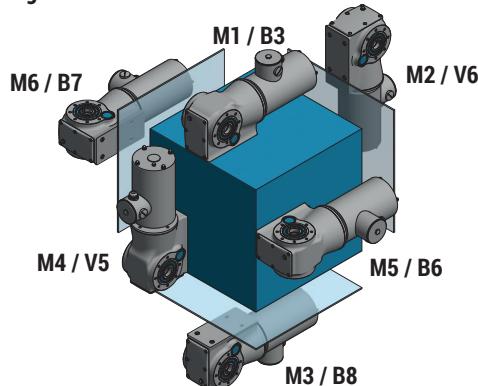


B5 motor

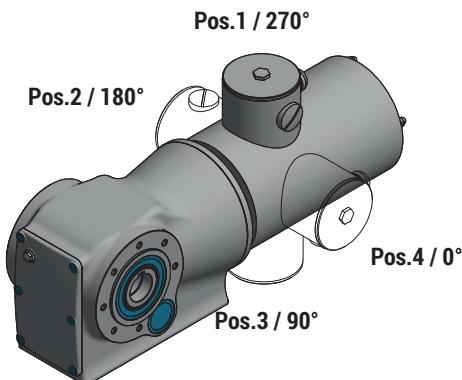


Extra information

Mounting Positions



Terminal Box Positions



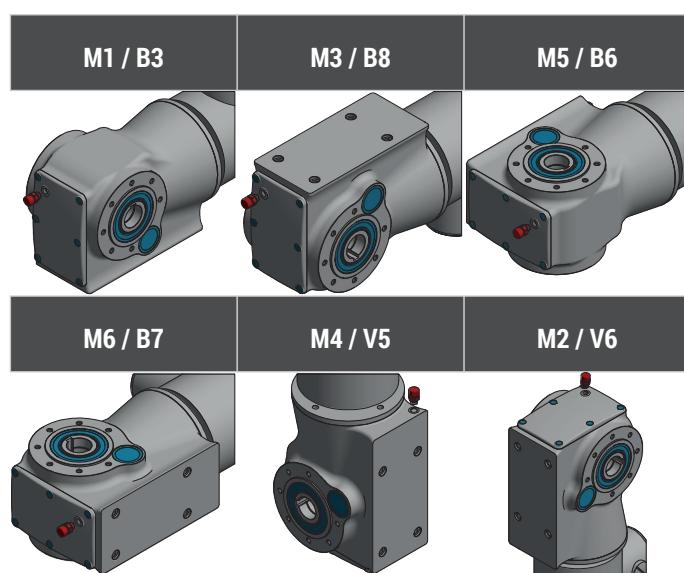
Lubrication Quantity

Oil Quantity in ML.	Mounting Position						
	Gearbox	M1 (B3)	M3 (B8)	M6 (B7)	M5 (B6)	M4 (V5)	M2 (V6)
FKA 38	900	900	1000	1000	1400	1000	
FKA 48	2000	2000	2000	2000	2700	2300	
FKA 68	2900	3750	3200	3200	4100	3100	
FKA 78	4000	5000	3750	3750	6000	3750	
FKA 88	5000	9000	8000	7500	11200	9000	

Lubrication Type

Lubrication Brand	Lubrication Type	
Matrix	Foodmax 460	Standard
Castrol	Optileb GT 460	Alternative
Bechem	Berusynth 460H1	Alternative
Shell	Casida Fluid GL460	Alternative
Mobil	SHC Cibus 460	Alternative

Debreather Positions



Weight

Gearbox B5T versions	Weight	Gearbox AM versions	Weight
FKA 38 B5T1	11.5 Kg	FKA 38 AM..	15.0 Kg
FKA 48 B5T2	16.0 Kg	FKA 48 AM..	20.0 Kg
FKA 68 B5T2	25.5 Kg	FKA 68 AM..	30 Kg
FKA 78 B5T3	43.0 Kg	FKA 78 AM..	50 KG
FKA 88 B5T4	*	FKA 88 AM..	*

* in development

Given values are an average and may vary depending on oil quantity.

**Dertec**

Einsteinpark 1
2171 TX Sassenheim
The Netherlands

T +31 71 409 2 409
E info@dertec.com

FKA Documentation - 1.0

3/3/2022

www.dertec.com

dertec®