



**FRC** 

# **FRC Helical gearbox**

With the food industry as a guideline, Dertec has developed a complete package of stainless steel drives.

The FRC Series Coaxial geared motor is a fine example of hygienic and easy to clean design.

The round shape and smooth surface contributes to the reduction of contamination building up and simplifies cleaning.

Using AISI 316 for the housing justifies the use of less reactive and therefore generally contributes to the surface water quality.

Dertec FRC coaxial gearboxes can be easily executed with different base plates and secondary flanges.

This makes them easily interchangeable with other brands available on the market.

Currently the 2-stage FRC coaxial gearboxes are available in 2 versions (FRC01 and FRC02) and suitable for IEC motor mounting.



#### **Main Features**

Made of high quality carefully electro polished Stainless Steel AISI 316 (mirror polished on request). The smooth design gives the gearbox a nice appearance, ready to suit all kinds of stainless steel machinery for the food industry.

#### Hardened shaft

All solid shafts are produced in duplex stainless steel AISI 2205. The special PNS surface treatment ensures enough hardness to collaborate with our special high temperature resistant blue shaft seals. The PNS treatment increases the lifetime of shaft / seal cooperation and helps to reduce wear on the shaft surface. By this, the gearbox achieves a longer drip free operation compared to standard shaft / seal combinations made of AISI 304 with NBR or FKM. The use of above combination offers all the positive characteristics of stainless steel and the surface hardness of a hardened shaft.

#### Blue shaft seals

Our high performance engineered shaft seals have a blue colour.

It is a well overthought feature for food industry applications.

It might be clear that the colour "blue" is a not existing organic colour.

In the context of food safety it is a common use to embed blue colours as these are very visible and easily to be recognised by vision scanning systems.

#### **Foodgrade lubrication**

All gearboxes are standard equipped with NSH H1 certified synthetic foodgrade lubrication. On request it can be supplied with a halal, kosher or nut free certification.

#### Laser engraved tag plate

To avoid dirt traps under the commonly used motor identification tag plate, all our motors and gearboxes are being equipped with a laser engraved tag plate.

Besides for the food safety this also prevents against possible loss of information because of taking away the tag plate or loosing the tag plate from the driveparts.

As a part of our standard procedure every drive is tested in our production facility in the Netherlands to ensure correct functioning.

#### **General specifications**

- Standard ratio's 3,82 : 1 to 54 : 1
- IEC motor adaption
- Standard solid shafts 20, 25 mm
- High efficiency of 94%
- Optional output flanges available
- · Stainless Steel AISI316
- Duplex stainless steel 2205 output shaft
- Interchangeable with euro sizes
- Designed and produced in the Netherlands
- Optional detachable feet to achieve different shaft heights
- Possible in combination with other gearboxes where the FRC gearbox funtions as a prestage gearbox

# **FRC Helical gearbox**



# **Product Characteristics**

FRC 01					
Ratio's	From 3.82 : 1				
ratios	To 53.33 : 1				
standard shaft	20 mm				
Torque	Max. 117 Nm				
Power	Max 1.5 kW				

FRC 02					
Davida	From 3.66 : 1				
Ratio's	To 54.00 : 1				
standard shaft	25 mm				
Torque	Max. 208 Nm				
Power	Max. 1.5 kW				

FRC01 flange						
Gearbox	Flange					
FRC01 FL120	SS 075 FL120					
FRC01 FL140	SS 075 FL140					
FRC01 FL160	SS 075 FL160					

FRC02 flange						
Gearbox	Flange					
FRC02 FL140	SS 085 FL140					
FRC02 FL160	SS 085 FL160					
FRC02 FL200	SS 085 FL200					

FRC01 foot						
Gearbox	Foot					
FRC01	M11					
FRC01	G1					

FRC02 foot					
Gearbox	Foot				
FRC02	M21				
FRC02	G2				

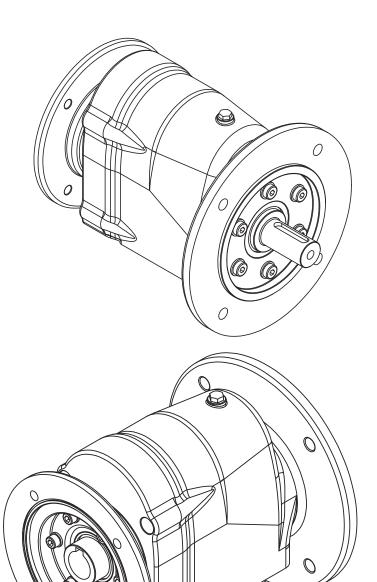


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0,75 - 1,1 kW 1,5 kW  General Dimensions  General dimensions  Foot & shaft  Flanges  B5T Flanges & Shafts  Optional foot  Extra information  Mounting Positions Lubrication Quantity Debreather Positions



#### **Basic Parameters**

#### Power P

The input power can be found in the "Gearbox Selection Tables", it represents the amount of kilowatts [kW] that can be safely transmitted into the gearbox.

$$P_1=\frac{P_2}{\eta}$$

= Input power (kW) = Output power (kW) = Gearbox efficiency (%)

#### Rotation speed *n* and gear ratio *i*

The gear ratio can be calculated with the input and output speed

$$i = \frac{n_1}{n_2}$$

i = Gear ratio

= Input speed in (rpm) n, = Output speed in (rpm)

#### Torque M

The output torque can be calculated with the input power, the efficiency and the output speed.

$$M_2 = \frac{9550 \cdot P_1 \cdot \eta}{n_2}$$

$$M_{2max} \ge M_2 \cdot f_{S_{gearbox}}$$

= Output torque (Nm) = Maximum output torque (Nm) = Input power (kW) = Output speed (rpm) = Gearbox efficiency (%)

= Service factor

#### Mass acceleration factor $f_a$

The mass acceleration factor is calculated with all the external mass moments of inertia and the mass moment of inertia from the motor.

$$f_a = \frac{J_c}{J_m}$$

= Mass acceleration factor

= All external mass moments of inertia [kg m<sup>2</sup>] = Mass moment of inertia on the motor end [kg m<sup>2</sup>]



If the mass acceleration factor  $f_a \ge 10$ , please contact us.

#### Efficiency of gearboxes $\eta$

The efficiency of gearboxes is mainly determined by the gear type, the gear ratio and the bearing friction. The efficiency of the gears at start-up and at sub-optimal operating speed is always lower than when the gears are running at the optimal operating speed. The gear shape of worm- and helical worm gearboxes causes more friction, thus a lower total efficiency. As a result of the higher friction, the temperature of worm gearboxes might also be higher than gearboxes with other gear types.

The efficiency of the different gear types can be found in the "Possible Geometrical Combinations".

For an approximate approach the following values can be used for the efficiency of gears at their (optimal) operational speed, beware these are generalized and can be different depending on the factors as discussed before.

For bevel-, helical- and parallel shaft gears the efficiency is in-between 94% (3-stage) and 96% (2-stage).

The efficiency of hypoid bevel gears is 90% (3-stage) and 92% (2-stage). For worm- and helical worm gears the efficiency depends on the gear ratio, incoming rotational speed and the temperature of the worm gearbox, the efficiency of the gears is between 40% and 90%.

To ensure the efficiency of the gears is optimal it is recommended but not limited to: Regularly change oil, use the optimal mounting position and use the gearbox at the optimal operating speed.

Choosing the right size gearbox for the application is recommended to achieve a better efficiency, at speeds below- and over the optimal operating speed the efficiency is lower than at optimal speeds and conditions.

#### Service factor fs<sub>min</sub> and fs<sub>gearbox</sub>

The service factor is a method to determine the effects of the driven machine or other application on the gearbox, with a sufficient level of accuracy for most applications. The minimal service factor (**fs**<sub>min</sub>) for a machine can be determined using the "Service factor graph". This minimum service factor is only an approximation, for the service factor for each gearbox, see the "Gearbox Selection Tables".



The minimal service factor (fs<sub>min</sub>) should always be lower than or equal to the actual service factor of the gearbox (fs<sub>nearbox</sub>).



fs<sub>min</sub> = Minimal determined service factor "Service factor graph"

gearbox

= Actual service factor for the gearbox "Gearbox Selection Tables"



The service factor for each gearbox ( $fs_{gearbox}$ ) is the critical service factor, and should always be equal to or higher than the minimum service factor ( $fs_{min}$ )!

#### **Switching frequency**

The switching frequency determines how often an application switches per hour.

The switching consists of: turning on/off, changing of speeds, changing of loads and braking

**z** = Switching frequency [1/h]

#### Load classification

There are three load classifications to be considered, they depend on the mass acceleration factor. The mass acceleration factor can be calculated, see "Mass acceleration factor f<sub>a</sub>"

**f** = Mass acceleration factor

The load classifications are split in three groups with each examples of the common applications for each load classification.

#### A: Uniform load, a mass acceleration factor of $f_a \le 0.3$

Examples of applications: Screw feeders for light materials, fans, assembly lines, conveyer belts for light materials, small mixers, light application elevators, cleaning machines, fillers, control machines.

#### **B:** Moderate shock load, mass acceleration of $f_1 \le 3$

Examples of applications: Winding devices, woodworking machine feeders, medium application elevators, balancers, medium mixers, conveyer belts for heavy materials, winches, sliding doors, fertilizer scrapers, packing machines, concrete mixers, crane mechanisms, milling cutters, folding machines, gear pumps.

**C:** Heavy shock load, mass acceleration factor of  $f_a \le 10$ . Examples of applications: Mixers for heavy materials, shears, presses, centrifuges, rotating supports, winches and lifts for heavy materials, heavy application elevators, grinding lathes, stone mills, bucket elevators, drilling machines, hammer mills, cam presses, folding machines, turntables, turntables, turntables, vibrators, shredders.

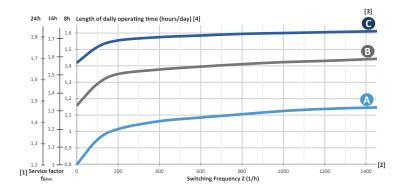
#### Service factor graph

The determined Minimum [1] service factor is based on [2] switching frequency, [3] load classification and [4] length of daily operating time.

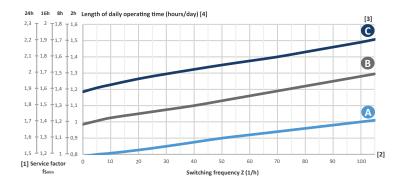


To get the expected service life from the gearbox,  $fs_{min} \le fs_{gearbox}$  see the "Gearbox Selection Tables" for the gearbox service factor

Service factor for a high Switching frequency [Z], used for all gearboxes:

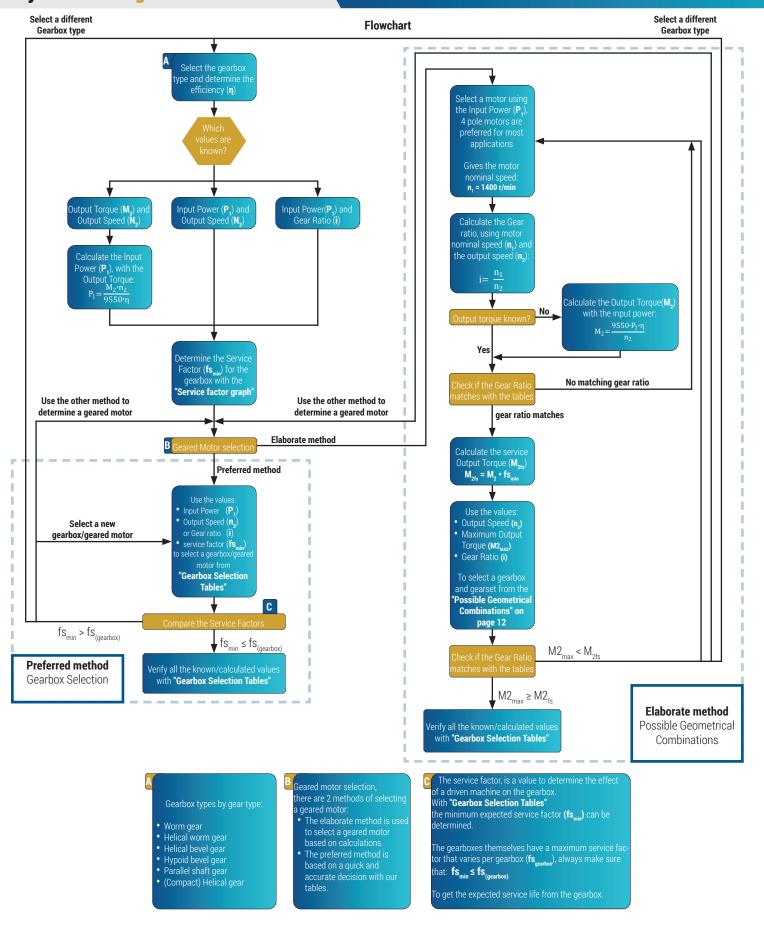


Service factor for low Switching frequency (Z), used mostly for worm- and helical worm gearboxes:



For worm gearboxes the ambient temperature has more influence on the service factor, the service factor should be adjusted as following:

Ambient temperature: =30~40°C,  $f_s$ •1,1 ~ 1,2 =40~50°C,  $f_s$ •1,3 ~ 1,4 =50~60°C,  $f_s$ •1,5 ~ 1,6



#### **Explanation of the flowchart**

#### **Gearbox selection type**

To select a gearbox the values for efficiency and the service factor are needed. These can be predicted by choosing the type of gearbox, "Possible Geometrical Combinations"

#### Which values are known?

There are three sets of values that can be known and which can be used to select the right gearbox and geared motor. These three sets of values are:

- · Output torque and speed
- · Input power and speed
- · Input power and gear ratio

For only knowing the output torque- and speed it is necessary to determine the input power with the following equation:

$$P_1 = \frac{M_2 \cdot n_2}{9550 \cdot \eta}$$

 $\begin{array}{ll} P_1 & \quad & \text{Input power [kW]} \\ M_2 & \quad & \text{Output torque [Nm]} \\ \eta & \quad & \text{Gearbox efficiency [\%]} \\ n_2 & \quad & \text{Rotational speed [rpm]} \end{array}$ 

#### **Determine the service factor**

Use the **"Service factor graph"** to determine the service factor.

#### Select a geared motor

There are two methods to select a gearbox and a geared motor:

The preferred method: This method is accurate and quick, this method only needs a basic calculation in when the input power is unknown.

**The elaborate method:** This method gives more insight and a more hands on approach in the selection process for a gearbox and geared motor. There are a few calculations that have to be done in this method.



If both methods don't give the correct results it can be possible that the gearbox and or motor are not correct for this application!

#### Preferred method:

#### **Use the "Gearbox Selection Tables"**

Use the Input power, output speed or gear ratio and the service factor to select the gearbox/geared motor.



Note: that the output torque is sufficiticated to your application

#### Check the service factor

Check if the determined service factor  $\mathbf{fs}_{\min}$  is smaller or equal to the service factor from the

"Gearbox Selection Tables" fs<sub>min</sub>≤ fs<sub>qearbox</sub>.

If  $fs_{min} > fs_{neathor}$  a different gearbox/geared motor should be selected if that is not possible then it is advised to check the other gearbox types...

If  $\mathbf{fs}_{\min} \le \mathbf{fs}_{\text{gearbox}}$  go to the next step and verify the results.

#### Verify the results

If the service factor  $\mathbf{fs}_{min}$  and  $\mathbf{fs}_{meantor}$  gives a valid result, verify the rest of the results with the tables from "Gearbox Selection Tables".

#### **Elaborate method:**

#### Select a motor

Select a motor from in the (Motor documentation).

4-pole motors are preferred for most applications. The given nominal motor speed of a 4-pole motor is n,=1400 rpm.

#### Calculate the gear ratio

If the gear ratio is known, the output speed **n**<sub>2</sub> needs to be calculated.

$$n_2 = \frac{n_1}{i}$$

With the nominal speed from the selected motor and known output speed the gear ratio can be calculated.

$$i = \frac{n_1}{n_2}$$

i = Gear ratio [-]

**n**<sub>1</sub> = Gearbox input speed [rpm] (equal to motor speed)

**n**<sub>2</sub> = Gearbox output speed [rpm]

#### Check if the output torque is known

If the output torque is known go to the next step.

If the output torque is unknown use the following calculation to determine the output torque:

$$P_1 = \frac{M_2 \cdot n_2}{9550 \cdot \eta}$$

P<sub>1</sub> = Input power [kW] M<sub>2</sub> = Output torque [Nm]

η = Gearbox efficiency [%]
η = Rotational speed [rpm]

#### Check the gear ratio

With the known or calculated gear ratio and the "Possible Geometrical Combinations", the gear ratio can be checked.

If the needed gear ratio is not in the list a different motor or gearbox should be selected.

#### Calculate the service output torque

With the determined service factor and the output torque, calculate the service output torque.

$$M_{2fs}=M_2 fs_{min}$$

**M**<sub>2fs</sub> = Service output torque [Nm]

**M<sub>2</sub>** = Output torque [Nm] **fs**<sub>min</sub> = Service Factor

#### **Use the Possible Geometrical Combinations tables**

Use the Output speed, Service output torque and gear ratio to determine a gearbox and gearset with the tables from the "Possible Geometrical Combinations".

#### Check the maximum output torque

Check if the maximum output torque in these tables matches the calculated service output torque. If the maximum torque is lower than the calculated service torque:  $\mathbf{M}_{2\text{max}} < \mathbf{M}_{2\text{fs}}$  it is advised to select a different motor or gearbox.

If  $\mathbf{M}_{2\text{max}} \ge \mathbf{M}_{2\text{fs}}$  go to the next step and verify the results.

#### Verify the results

If the maximum output torque matches the tables and gives a valid result, then verify the values from the tables with the calculated values and make a selection for the gearbox/geared motor.

#### **Example 1: Preferred method**

#### **Known parameters:**

Moderate shock load, operational 16 hours a day, Switching frequency of 200 times per hour.

This example uses a different gearbox type but is generally applicable

#### Gearbox selection type

A hypoid bevel gearbox is selected. The estimated efficiency *η≈90% to 94%*. For a more accurate efficiency look it up in the "Possible Geometrical Combinations".

When in doubt use the lowest estimated efficiency.

#### Which values are known?

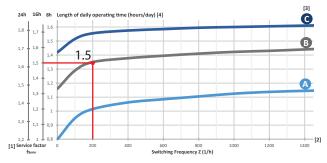
- · Output torque- and speed
- Input power- and speed
- · Input power and gear ratio

 $M_2 = 110Nm$  $n_2 = 29 rpm$ 

Looking up the output speed and output torque in the **"Possible Geometrical Combinations" on page 15** tables gives an efficiency of: η≈92% With the output torque- and speed it is necessary to determine the input power with the following equation:

$$P_1 = \frac{M_2 \cdot n_2}{9550 \cdot \eta} = \frac{110 \cdot 29}{9550 \cdot 0,92} = 0,363 \text{ kW}$$

#### Determine the safety factor



#### Select the 'Elaborate method' or the 'Preferred method'

Preferred method is chosen.

P <sub>1n</sub> [kW]	n <sub>2</sub> min <sup>-1</sup>	M <sub>2n</sub> [Nm]	i	F <sub>r2</sub> [N]	fs		
0.37	23	140	60.50	3430	1.40		
	29	113	48.71	3190	1.80		
	36	91	39.29	2970	2.00		
	46	70	30.31	2720	2.80	FK38B IEC71	712-4 B14a
	57	57	24.44	2530	3.20		
	69	47	20.25	2380	3.20		
	95	34	14.67	2130	3.20		

#### Check the service factor

fs<sub>min</sub>=1,5 fs<sub>(gearbox)</sub>=1,8

#### Check if the following is true

fs<sub>min</sub>≤ fs<sub>gearbox</sub> Yes, because **1,5 < 1,8** 

#### Verify the results

Needed Torque: 110 Nm, available torque in selected gearbox: 113 Nm

Needed output speed: 29 rpm, available output speed in selected gearbox: 29 rpm

Calculated Input power: 0,363 kW, available input power in selected gearbox: 0.37 kW

Service factor:  $fs_{min} \le fs(gearbox) = 1,5<1,8$ 

So the choice of gearbox/geared motor is: FK38B IEC71 / 712-4 B14a.



It is recommended to select a gearbox or geared motor that fits the application. Choosing a gearbox or geared motor that is too light or too heavy can cause damage (to the machine) and shorten the expected service life of the gearbox/geared motor!

#### **Example 2: Eleborate method**

This example uses a different gearbox type but is generally applicable

#### **Known parameters:**

**P1** Input power [kW] = **0.55kW** 

**i** gear ratio = **30:1** 

Heavy shock load, operational **24 hours a day**, switching frequency of **800 times per hour**.

#### Gearbox selection type

A hypoid bevel gearbox is selected. The estimated efficiency *η≈90% to 94%*. For a more accurate efficiency look it up in the "Possible Geometrical Combinations"

When in doubt use the lowest estimated efficiency.

#### Which values are known?

· Output torque- and speed

P<sub>1</sub> = **0.55 kW** 

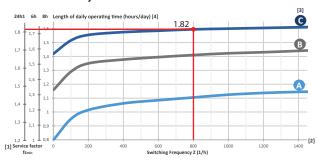
Input power- and speed

i = **30:1** 

Input power and gear ratio

Looking up the output speed and output torque in the "Possible Geometrical Combinations" tables gives an efficiency of: n≈94%

#### Determine the safety factor



#### Select the elaborate or the Simple method

Elaborate method is chosen

#### Select a motor

Check the "Possible Geometrical Combinations", which motor is preferred. In this example an IEC80 B14a motor is preferred.



The choice of motor is based on a 4-pole motor, which means an input speed of 1400 rpm. However it is possible to choose from a wide range of motors.

Calculate the output speed

$$i = \frac{n_1}{n_2} \rightarrow n_2 = \frac{n_1}{i} \rightarrow \frac{1400 \text{ rpm}}{30} = 46,67 \text{ rpm}$$

#### Check of the output torque is known

The output torque is not known yet, so it needs to be calculated with the known values

$$M = \frac{9550 \cdot P \cdot \eta}{2} = \frac{9550 \cdot 0,55 \cdot 0,90}{46,67 \ rpm} \quad 101,3 \ Nm$$

#### Check the gear ratio

To check the gear ratio, look in the **"Possible Geometrical Combinations"** tables for the preferred gearbox. As seen below, the gear ratio and output speed match with this gearbox. The preferred motor is also possible with this gearbox type.

**FK 28 B** 

Maximum torque = 130 Nm @ N1 = 1400 rpm

<b>n</b> <sub>2</sub> [min <sup>-1</sup> ]	M <sub>2max</sub> [Nm]	F <sub>r2</sub> [N]		i	η%	IEC 63 B5	IEC 71 B14a	IEC 80 B14a	IEC 90 B14a
35	130	2610	40	40.09	94	<b>4</b>	<	<b>*</b>	
48	130	2350	30	29.33	94	<	<	<b>*</b>	
59	130	2200	25	24.07	94	<	<	<b>*</b>	<b>₩</b>

#### Calculate the service output torque

Use the determined service factor and the calculated output torque.

$$M_{2fs} = M_2 \cdot fs_{min} \rightarrow 101,3 \text{ Nm} \cdot 1,82 = 184,37 \text{ Nm}$$

**Use the Possible Geometrical Combinations tables** 

**FK 28 B** 

<u>Maximum torque = **130 Nm**</u> @ N1 = 1400 rpm

	<b>n</b> 2 [Min <sup>-1</sup> ]	M <sub>2max</sub> [Nm]	F <sub>r2</sub> [N]		i	η%	IEC 63 B5	IEC 71 B14a	IEC 80 B14a	IEC 90 B14a
	35	130	2610	40	40.09	94	<	<	<b>*</b>	
I	48	130	2350	30	29.33	94	<	<	<b>*</b>	
Ī	59	130	2200	25	24.07	94	<b>4</b>	<b>₩</b>	<	<

#### Check the maximum output torque

With the known values and the selected gearbox, we can determine that the following values apply:

 $n_2 = 48 \text{ rpm} \approx 46.67 \text{ rpm [calculated]}$ 

I = 30 = 30 [known]

M2fs = 101,3 Nm [calculated]

So the determined gearbox has enough output torque for the application 130 Nm, but when we look at the service output torque, it is not recommended to choose this gearbox with this service factor and service output torque.

$$M_{2fs} = 184,37 \text{ Nm [calculated]}$$

$$M_{2max} < M_{2fs} \rightarrow 130 \text{ Nm} < 184,37 \text{ Nm}$$



It is recommended to choose another gearbox, the easiest way to do this is to look for a bigger gearbox within the same gearbox type.

#### Selecting a new gearbox

It is recommended to match the calculated results as before, but look for a higher maximum torque. Try to select a maximum torque that still matches the application, it is not recommended to select a gearbox with more maximum torque than the application needs.

**FK 38 B** 

Maximum torque = 200 Nm @ N1 = 1400 rpm

<b>n</b> <sub>2</sub> [Min <sup>-1</sup> ]	M <sub>2max</sub> [Nm]	F <sub>r2</sub> [N]		i	η%	IEC 63 B5	IEC 71 B14a	IEC 80 B14a	IEC 90 B14a
36	200	2970	40	39.29	94	<b>*</b>	<b>✓</b>	<b>*</b>	<b>*</b>
47	200	2720	30	30.31	94	<	<	<b>*</b>	<
58	200	25030	25	24.44	94		<b>*</b>	<b>4</b>	<b>*</b>

#### Verify the results

With the table for the FK38B gearbox, we can determine the following.

 $n_2 = 47 \text{ rpm} \approx 46.67 \text{ rpm [calculated]}$ 

i = 30 = 30 = [known]

M<sub>2</sub> = 101,3 Nm [calculated]

M<sub>260</sub> = 184,37 Nm [calculated]

Check if the maximum output torque is higher than the service output torque.

So this gearbox can be used for the application, because the service output torque is lower than the maximum output torque.

#### The recommended gearbox with motor is:

For a gearbox, a FK38B with a true gear ratio of 30,31 and for a motor, the IEC80 B14a is possible.



It is recommended to select a gearbox or geared motor that fits the application. Choosing a gearbox or geared motor that is too light or too heavy can cause damage (to the machine) and shorten the expected service life of the gearbox/geared motor

#### Overhung and axial loads

#### **Determing overhung loads**

Each transmission element has a transmission element factor **f**, this factor is different for each element.

In order to properly use transmission elements, always make sure that they are aligned properly on the shaft of the gearbox and or the shaft of the machine or other application. It is important to check that the transmission element is mounted properly before use, the element might cause problems in dynamic situations if this isn't checked

	M-2000	fz
$F_r =$	$d_0$	'IZ

F<sub>r</sub> = overhung load [N]

M = Torque [Nm]
d = Mean diameter of the mounted element [mm]

**F**, = Element factor [see table above]

Transmission elements	Transmission elements Factor Fz	Comments
	1.00	≥ 17 Teeth
Gears	1.15	< 17 Teeth
	1.00	≥ 20 Teeth
Chain sprockets	1.25	< 20 Teeth
	1.40	< 13 Teeth
Narrow V-belt Pulleys	1.75	Influence of the tensile force
Flat Belt Pulleys	2.50	Influence of the tensile force
Toothed Belt Pulleys	2.50	Influence of the tensile force

#### Rated bearing service life

The rated bearing service life  $L_{10h}$  (in hours, according to **ISO 281**) is used to calculate the estimated bearing life in hours. For special operating conditions the modified service life should be used.

$$L_{10h} = \frac{10^6}{60 \cdot n_2} \cdot \left(\frac{C}{F_r}\right)$$

**L**<sub>10h</sub> = Rated service life [hour]

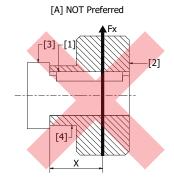
C = Basic dynamic load rating, bearing [kN] F = Equivalent dynamic load, bearing [kN]

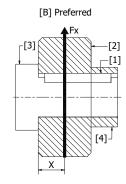
 $\rho$  = Exponent for the life equation,  $\rho$ =3 for ball bearings,  $\rho$ =10/3 for roller bearings

**n**<sub>2</sub> = Gearbox output speed [rpm]

#### Preferred mounting for overhung loads

The preferred way of mounting the overhung load for sprockets, gears and other transmissions is with the hub [4] at the end of the shaft [3] and the sprocket/gear [2] against the shoulder, see [B] in the figure below. This method ensures a better load distribution on the end of the shaft.

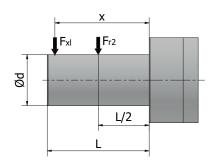


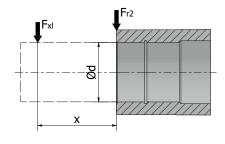


nr.	Part Name
[1]	Key
[2]	Sprocket / Gear
[3]	Solid shaft
[4]	Hub
[Fx]	Radial Force on the Sprocket / Gear
[x]	Distance to center of mass and force

#### Overhung load conversion for off-centre force applications

The rated bearing life is the basis for determining the permissible overhung load. The permissible overhung loads for foot mounted gearboxes with solid shafts can be calculated with the following calculation.





$$F_{xL} = F_{r2} \cdot \frac{a}{b+x}$$

 $\mathbf{F}_{\mathbf{xL}}$  = Permitted overhung load based on bearing service life[N]

 $\mathbf{F}_{,2}$  = Permitted overhung load (x=L/2) for foot mounted gearboxes according to the selection tables [N]

= Maximum permitted overhung load (x=L/2) for foot mounted gearboxes according to the sellection tables [N]

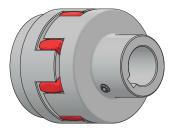
**x** = Distance from the shaft shoulder to the applied force [mm]

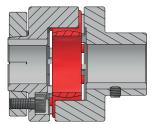
**a,b ød, L** = Gear unit constant for overhung load conversions [mm]

The values in table are for the foot mounted gearboxes with solid shaft only, the measurements are for the standard shafts.

FV	a [mm]	b [mm]	Ød [mm]	L [mm]	Fr2 max [N]	FRC	a [mm]	b [mm]	Ød [mm]	L
FV 030	65	50	14	30	1830	FRC 01	103	83	20	
FV 040	84	64	18	40	3490	FRC 02	116,5	91,5	25	
FV 050	101	76	25	50	4840	FK	a [m	m] b [m	m] Ød [m	m]
FV 063	120	95	25	50	6270	FK 28 B/	C 10	4 78	25	
FV 075	131	101	28	60	7380	FK 38 B/	C 11	8 93	25	
FV 090	162	122	35	80	8180	FK 48 B/	C 13	1 10	28	
FKA	a [mm]	b [mm]	Ød [mm]	L [mm]		FK 58 B/	C 15	9 119	35	
FKA 38	123,5	98,5	25	50		FS(A)	a [mm	b [mm]	Ød [mm	Ī
FKA 48	153,5	123,5	30	60		FS(A) 38	118,5	98,5	20	Т
FKA 68	181,3	141,3	40	80		FS(A) 48	130	105	25	
FKA 78	215,8	165,8	50	100		FS(A) 58	150	120	30	
FKA 88	252	192	60	120		FS(A) 68	184	149	35	
FFA	a [mm]	b [mm]	Ød [mm]	L [mm]		FR	a [mm]	b [mm]	Ød [mm]	L
FFA 38	123,5	98,5	25	50		FR 38	118	93	25	
FFA 48	153,5	123,5	30	60		FR 48	137	107	30	
FFA 68	181,3	141,3	40	80		FR 68	168,5	133,5	35	
FFA 78	215.8	165.8	50	100						

#### The use of couplings







Example of a flexible coupling

Couplings are usually needed when a gearbox is rigidly mounted to a machine or other application. A coupling offers some room for misalignment that may be present or develop during use of the gearbox.



Not all misalignments can be statically determined, some may develop during dynamic processes are only present during use of the gearbox

Couplings give room for these misalignments and ensure the service life of the bearings inside of the gearbox, by offering a bit more room for error when there are misalignments.

There are different types of couplings that can be used in such applications, one example is a flexible coupling ,see: example of a flexible coupling. Flexible couplings often have three parts, one for the shaft of the machine or application, one for the shaft of the gearbox and a part that gives flexibility. The flexible part is often made of rubber or another kind of polymer.



Note: A coupling slightly increases the temperature of the shafts, due to friction and slightly decreases the efficiency of the gearbox.

#### Mounting of couplings

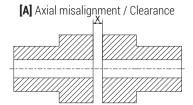
To properly mount the couplings and prevent excessive wear on the gearbox, it is necessary to mount the couplings correctly. To mount a coupling properly please pay attention to the following types of misalignment.

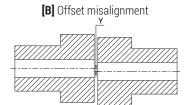


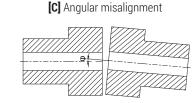
Note: The amount of allowable misalignment is often specified in the coupling datasheet, from the coupling manufacturer



Never mount couplings onto the shaft by hitting them with a hammer, this can cause damage to the gearbox bearings and can reduce the gearbox service life







#### [A] Horizontal misalignment/Clearance:



Note: For the allowable clearance see the coupling manufacturers data sheet.

#### [B] Axial misalignment:

Make sure that the axial misalignment [Y] is as close to 0 as possible, in general axial misalignment will cause wear when the misalignment is too big.

#### [C] Angular misalignment:

Make sure the angular misalignment  $[\phi]$  is as close to 0 (degrees) as possible, excessive angular misalignment will cause damage.



Couplings allow small misalignments, but excessive misalignment and couplings that aren't mounted properly can still cause damage to the gearbox and or machine or other applications.

# Possible Geometrical Combinations

# **Possible Geometrical Combinations**

FRC 01

Maximum Torque = 120 Nm @ N1 = 1400 min<sup>-1</sup>

Maximum	rorque	C 12011111 @ 111 1 10011111						
n2 [Min-1]	M2max [Nm]	Fr2 [N]	i	η%	IEC63 B5	IEC71 B14A	IEC80 B14A	IEC90 B14A
26	120	2600	53,33	96 %	V	V		
31	120	2600	45,89	96 %	V	V	V	
35	120	2600	40,10	96 %	٧	V	V	
39	120	2560	35,47	96 %	V	V	V	
49	120	2380	28,50	96 %	V	V	V	
59	120	2230	23,56	96 %	V	V	V	
71	120	2100	19,83	96 %	V	V	V	V
78	90	2030	17,86	96 %	V	V	V	
96	120	1900	14,62	96 %	V	V	V	V
101	90	1860	13,80	96 %	٧	V	V	V
118	120	1770	11,90	96 %	٧	V	V	V
143	120	1660	9,81	96 %	V	V	V	
153	80	1630	9,17	96 %	V	V	V	
181	80	1540	7,72	96 %	V	V	V	
246	70	1390	5,69	96 %	V	V	V	V
302	70	1290	4,63	96 %	V	V	V	V

FRC 02

Maximum Torque = 200 Nm @ N1 = 1400 min<sup>-1</sup>

махітит	Torque	= 200 N	m @ N I	= 14001	nin'			
n2 [Min-1]	M2max [Nm]	Fr2 [N]	i	η%	IEC63 B5	IEC71 B14A	IEC80 B14A	IEC90 B14A
26	200	4500	54,00	96 %	V	V	V	
30	200	4500	46,46	96 %	V	V	V	
34	200	4500	40,60	96 %	V	V	V	
39	200	4270	35,91	96 %	V	V	V	
48	200	3970	28,88	96 %		V	V	
59	200	3730	23,85	96 %		V	V	
70	200	3520	20,08	96 %		V	V	
82	140	3330	17,10	96 %		V	V	
95	200	3180	14,81	96 %		V	V	
106	140	3060	13,21	96 %			V	
116	200	2970	12,05	96 %			V	
141	200	2780	9,93	96 %			V	
159	120	2670	8,78	96 %			V	
189	120	2520	7,39	96 %			V	
257	100	2280	5,45	96 %			V	
316	100	2120	4,43	96 %				
383	80	1990	3,66	96 %				V



Possible (	Geometrical	<b>Combinations</b>
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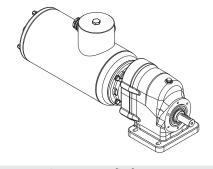
# **Possible Geometrical Combinations**

#### 0,12 - 0,18 kW

P1 [kW]	n2 [Min-1]	M2 [Nm]	i	Fr2 [N]	fs gear- box			
	26	42	53,33	2600	2,9			
	31	36	45,89	2600	3,3			
	35	32	40,1	2600	3,8			
	39	28	35,47	2560	4,3			
	49	22	28,5	2380	5,4			
	59	18,5	23,56	2230	6,5			
	71	15,6	19,83	2100	7,7			
	78	14	17,86	2030	6,4			
0,12	96	11,5	14,62	1900	10,4	FRC 01 IEC63	631-4 B5	
	101	10,8	13,8	1860	8,3			
	118	9,4	11,9	1770	12,8			
	143	7,7	9,81	1660	15,6			
	153	7,2	9,17	1630	11,1			
	181	6,1	7,72	1540	13,2			
	246	4,5	5,69	1390	15,7			
	302	3,6	4,63	1290	19,2			
	366	3	3,82	1210	23,3			
	26	63	53,33	2600	1,9		-	
	31	54	45,89	2600	2,2			
	35	47	40,1	2600	2,5			
	39	42	35,47	2560	2,9			
	49	34	28,5	2380	3,6			
	59	28	23,56	2230	4,3			
	71	23	19,83	2100	5,1			
	78	21	17,86	2030	4,3			
	96	17,2	14,62	1900	7	FRC 01 IEC63	632-4 B5	
	101	16,3	13,8	1860	5,5			
	118	14	11,9	1770	8,6			
	143	11,6	9,81	1660	10,4			
0,18	153	10,8	9,17	1630	7,4			
	181	9,1	7,72	1540	8,8			
	246	6,7	5,69	1390	10,4			
	302	5,5	4,63	1290	12,8			
	366	4,5	3,82	1210	15,5			
	16,9	98	53,33	2600	1,2			
	19,6	84	45,89	2600	1,4	FRC 01 IEC71		
	22	74	40,1	2600	1,6			
	25	65	35,47	2600	1,8		711-6 B14a	
	32	52	28,5	2600	2,3			
	38	43	23,56	2580	2,8			
	45	36	19,83	2440	3,3			
	50	33	17,86	2360	2,7			
	26	64	54	4500	3,1	FRC 02 IEC63	632-4 B5	

0,18 - 0,25 kW

[kW]	n2 [Min-1]	M2 [Nm]	i	Fr2 [N]	fs gear- box		
	16,7	99	54	4500	2		
	19,4	85	46,46	4500	2,3		
0,18	22	74	40,6	4500	2,7	FRC 02 IEC71	711-6 B14a
	25	66	35,91	4500	3		
	31	53	28,88	4500	3,8		
	26	87	53,33	2600	1,4		
	31	75	45,89	2600	1,6		
	35	66	40,1	2600	1,8		
	39	58	35,47	2560	2,1		
	49	47	28,5	2380	2,6		
	59	39	23,56	2230	3,1		
	71	32	19,83	2100	3,7		
	78	29	17,86	2030	3,1		
	96	24	14,62	1900	5	FRC 01 IEC71	711-4 B14a
	101	23	13,8	1860	4		
	118	19,5	11,9	1770	6,2		
	143	16,1	9,81	1660	7,5		
	153	15	9,17	1630	5,3		
	181	12,6	7,72	1540	6,3		
	246	9,3	5,69	1390	7,5		
	302	7,6	4,63	1290	9,2		
	366	6,3	3,82	1210	11,2		
	19,6	117	45,89	2600	1		
	22	102	40,1	2600	1,2		
	25	90	35,47	2600	1,3		
	32	73	28,5	2600	1,7		
),25	38	60	23,56	2580	2		
	45	51	19,83	2440	2,4		
	50	45	17,86	2360	2		
	62	37	14,62	2200	3,2		
	65	35	13,8	2160	2,6	FRC 01 IEC71	712-6 B14a
	76	30	11,9	2060	4		
	92	25	9,81	1930	4,8		
	98	23	9,17	1890	3,4		
	117	19,7	7,72	1780	4,1		
	158	14,5	5,69	1610	4,8		
	194	11,8	4,63	1500	5,9		
	236	9,7	3,82	1410	7,2		
	26	88	54	4500	2,3		
	30	76	46,46	4500	2,6		=
	34	66	40,6	4500	3	FRC 02 IEC71	711-4 B14a
	39	59	35,91	4270	3,4		
	16,7	138	54	4500	1,5		
	19,4	118	146,46	4500	1,7		
	22	103	40,6	4500	1,9	FRC 02 IEC71	712-6 B14a
	25	91	35,91	4500	2,2	-	
	31	74	28,88	4500	2,7		



 $\begin{array}{c} \boldsymbol{P}_{1n} \\ \boldsymbol{n}_{2} \\ \boldsymbol{M}_{2n} \end{array}$ 

<sup>=</sup> Rated Motor Power [kW] = Output Speed [min<sup>-1</sup>] = Rated Output torque [Nm]

<sup>=</sup> Maximum permissible output torque [Nm] = Permitted Overhung Load Output Side [N] = Gear unit Ratio

<sup>=</sup> Transmission Efficiency % = Service Factor

#### 0,37 kW

U,31 KW								
P1 [kW]	n2 [Min-1]	M2 [Nm]	i	Fr2 [N]	fs gear- box			
	31	111	45,89	2600	1,1			
	35	97	40,1	2600	1,2			
	39	86	35,47	2560	1,4			
	49	69	28,5	2380	1,7			
	59	57	23,56	2230	2,1			
	71	48	19,83	2100	2,5			
	78	43	17,86	2030	2,1			
	96	35	14,62	1900	3,4	EDO 01 JE071	710 4 01 4	
	101	33	13,8	1860	2,7	FRC 01 IEC71	712-4 B14a	
	118	29	11,9	1770	4,2			
	143	24	9,81	1660	5			
	153	22	9,17	1630	3,6			
	181	18,7	7,72	1540	4,3			
	246	13,8	5,69	1390	5,1			
	302	11,2	4,63	1290	6,2			
	366	9,3	3,82	1210	7,6			
	32	107	28,5	2600	1,1			
	38	89	23,56	2580	1,4			
	45	75	19,83	2440	1,6			
	50	67	17,86	2360	1,3			
	62	55	14,62	2200	2,2	FRC 01 IEC80	801-6 B14a	
0,37	65	52	13,8	2160	1,7	FNC UT IECOU	001-0 D14a	
U,SI	76	45	11,9	2060	2,7			
	92	37	9,81	1930	3,2			
	98	35	9,17	1890	2,3			
	117	29	7,72	1780	2,7			
	26	131	54	4500	1,5			
	30	113	46,46	4500	1,8			
	34	98	40,6	4500	2			
	39	87	35,91	4270	2,3			
	48	70	28,88	3970	2,9	FRC 02 IEC71	712-4 B14a	
	59	58	23,85	3730	3,5			
	70	49	20,08	3520	4,1			
	82	41	17,1	3330	3,4			
	95	36	14,81	3180	5,6			
	16,7	204	54	4500	1	FRC 02 IEC80		
	19,4	175	46,46	4500	1,1			
	22	153	40,6	4500	1,3			
	25	135	35,91	4500	1,5			
	31	109	28,88	4500	1,8		801-6 B14a	
	38	90	23,85	4320	2,2			
	45	76	20,08	4080	2,6			
	53	64	17,1	3860	2,2			
	68	50	13,21	3550	2,8			

#### 0 55 kW

0,55 kW							
P1 [kW]	n2 [Min-1]	M2 [Nm]	i	Fr2 [N]	fs gear- box		
	49	103	2850	2380	1,2		
	59	85	23,56	2230	1,4		
	71	71	19,83	2100	1,7		
	78	64	17,86	2030	1,4		
	96	53	14,62	1900	2,3		
	101	50	13,8	1860	1,8		
	118	43	11,9	1770	2,8	FRC 01 IEC80	801-4 B14a
	143	35	9,81	1660	3,4		
	153	33	9,17	1630	2,4		
	181	28	7,72	1540	2,9		
	246	20	5,69	1390	3,4		
	302	16,7	4,63	1290	4,2		
	366	13,8	3,82	1210	5,1		
	45	111	19,83	2440	1,1		
	62	82	14,62	2200	1,5		802-6 B14a
	65	77	13,8	2160	1,2		
0,55	76	67	11,9	2060	1,8		
	92	55	9,81	1930	2,2	FD0 01 1F000	
	98	51	9,17	1890	1,6	FRC 01 IEC80	
	117	43	7,72	1780	1,8		
	158	32	5,69	1610	2,2		
	194	26	4,63	1500	2,7		
	236	21	3,82	1410	3,3		
	26	194	54	4500	1		
	30	167	46,46	4500	1,2		
	34	146	40,6	4500	1,4	FRC 02 IEC80	
	39	129	35,91	4270	1,5		
	48	104	28,88	3970	1,9		001 4 01 4
	59	86	23,85	3730	2,3		801-4 B14a
	70	72	20,08	3520	2,8		
	82	62	17,1	3330	2,3		
	95	53	14,81	3180	3,7		
	106	48	13,21	3060	2,9		

M<sub>2max</sub> F<sub>r2</sub>

<sup>=</sup> Maximum permissible output torque [Nm] = Permitted Overhung Load Output Side [N] = Gear unit Ratio

<sup>=</sup> Transmission Efficiency % = Service Factor

#### 0,55 - 0,75 kW

0,00 0,	7 3 KW						
P1 [kW]	n2 [Min-1]	M2 [Nm]	i	Fr2 [N]	fs gear- box		
	25	201	35,91	4500	1		
	31	162	28,88	4500	1,2		
	38	134	23,85	4320	1,5		
0.55	45	113	20,08	4080	1,8	EDO 00 15000	000 6 014
0,55	53	96	17,1	3860	1,5	FRC 02 IEC80	802-6 B14a
	61	83	14,81	3680	2,4		
	68	74	13,21	3550	1,9		
	103	49	8,78	3090	2,4		
	59	116	23,56	2230	1		
	71	97	19,83	2100	1,2		
	78	88	17,86	2030	1		
	96	72	14,62	1900	1,7		
	101	68	13,8	1860	1,3		
	118	58	11,9	1770	2,1	FRC 01 IEC80	002 4 P14o
	143	48	9,81	1660	2,5	FNG UT IEGOU	802-4 B14a
	153	45	9,17	1630	1,8		
	181	38	7,72	1540	2,1		
	246	28	5,69	1390	2,5		
	302	23	4,63	1290	3,1		
	366	18,8	3,82	1210	3,7		
	62	112	14,62	2200	1,1		90S-6 B14a
	76	91	11,9	2060	1,3		
	92	75	9,81	1930	1,6		
	98	70	9,17	1890	1,1	FRC 01 IEC90	
0,75	117	59	7,72	1780	1,4	THE OTTEGE	903-0 D14a
	158	43	5,69	1610	1,6		
	194	35	4,63	1500	2		
	236	29	3,82	1410	2,4		
	34	199	40,6	4500	1		
	39	176	35,91	4270	1,1		
	48	142	28,88	3970	1,4		
	59	117	23,85	3730	1,7		
	70	99	20,08	3520	2		
	82	84	17,1	3330	1,7		
	95	73	14,81	3180	2,7	FRC 02 IEC80	FRC 02 IEC80
	106	65	13,21	3060	2,2		
	116	59	12,05	2970	3,4		
	141	49	9,93	2780	4,1		
	159	43	8,78	2670	2,8		
	189	36	7,39	2520	3,3		
	257	27	5,45	2280	3,7		

075 - 11kW

P1 [kW]	n2 [Min-1]	M2 [Nm]	i	Fr2 [N]	fs gear- box		
	38	182	23,85	4320	1,1	,	
	45	153	20,08	4080	1,3		
	61	113	14,81	3680	1,8		
	68	101	13,21	3550	1,4		
0,75	75	92	12,05	3440	2,2	FRC 02 IEC90	90S-6 B14a
	91	76	9,93	3220	2,6		
	103	67	8,78	3090	1,8		
	122	56	7,39	2920	2,1		
	165	42	5,45	2640	2,4		
	96	105	14,62	1900	1,1		
	118	86	11,9	1770	1,4		
	143	71	9,81	1660	1,7		
	153	66	9,17	1630	1,2	EBC 01 IEC00	90S-4 B14a
	181	56	7,72	1540	1,4	FRC 01 IEC90	
	246	41	5,69	1390	1,7		
	302	33	4,63	1290	2,1		
	366	28	3,82	1210	2,5		
	92	110	9,81	1930	1,1		
	158	64	5,69	1610	1,1	EDO 01 JE000	00L C D1.4-
	194	52	4,63	1500	1,3	FRC 01 IEC90	90L-6 B14a
	236	43	3,82	1410	1,6		
	59	172	23,85	3730	1,2		
	70	145	20,08	3520	1,4		
	95	107	14,81	3180	1,9		
1,1	106	95	13,21	3060	1,5		
	116	87	12,05	2970	2,3		
	141	72	9,93	2780	2,8	FRC 02 IEC90	90S-4 B14a
	159	63	8,78	2670	1,9		
	189	53	7,39	2520	2,3		
	257	39	5,45	2280	2,5		
	316	32	4,43	2120	3,1		
	383	26	3,66	1990	3		
	61	166	14,81	3680	1,2		
	75	135	12,05	3440	1,5		
	91	111	9,93	3220	1,8	EDO 00 IE000	
	103	98	8,78	3090	1,2		001 C D3 4
	122	83	7,39	2920	1,4	FRC 02 IEC90	90L-6 B14a
	165	61	5,45	2640	1,6		
	203	50	4,43	2460	2		
	246	41	3,66	2310	2		

 $\begin{array}{c} \boldsymbol{P}_{1n} \\ \boldsymbol{n}_{2} \\ \boldsymbol{M}_{2n} \end{array}$ 

<sup>=</sup> Rated Motor Power [kW] = Output Speed [min<sup>-1</sup>] = Rated Output torque [Nm]

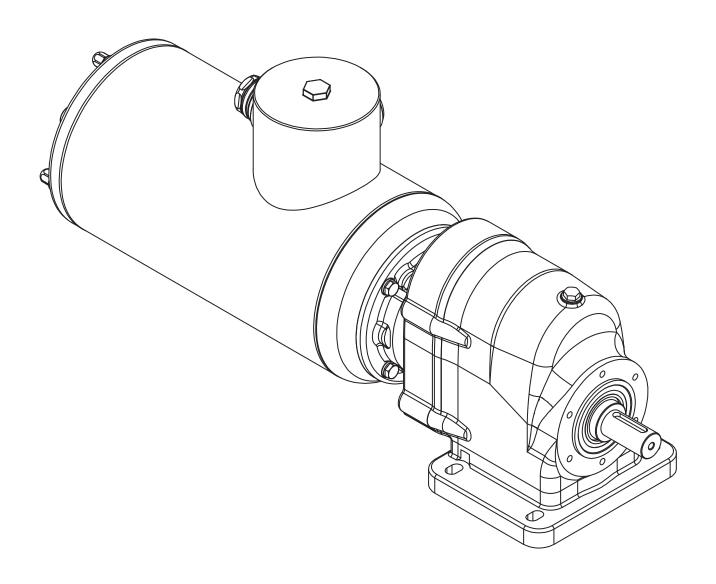
M<sub>2max</sub> F<sub>r2</sub>

<sup>=</sup> Maximum permissible output torque [Nm] = Permitted Overhung Load Output Side [N] = Gear unit Ratio

<sup>=</sup> Transmission Efficiency % = Service Factor

#### 1,5 kW

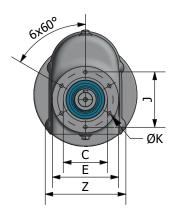
P1 [kW]	n2 [Min-1]	M2 [Nm]	i	Fr2 [N]	fs gear- box				
	118	117	11,9	1770	1				
	143	96	9,81	1660	1,2				
	181	76	7,72	1540	1,1	EDO 01 JE000	001 4 D14-		
	246	56	5,69	1390	1,3	FRC 01 IEC90	90L-4 B14a		
	302	45	4,63	1290	1,5				
	366	38	3,82	1210	1,9				
1.5	95	145	14,81	3180	1,4				
1,5	116	118	12,05	2970	1,7				
	141	98	9,93	2780	2,1				
	159	86	8,78	2670	1,4	EDO 00 15000	001 4 01 4		
	189	73	7,39	2520	1,7	FRC 02 IEC90	90L-4 B14a		
	257	54	5,45	2280	1,9				
	316	44	4,43	2120	2,3				
	383	36	3,66	1990	2,2				

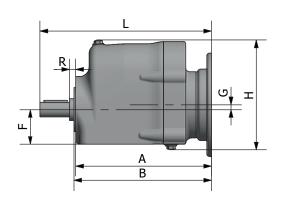


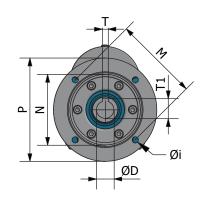
# **General Dimensions**

# **General Dimensions**

#### **General dimensions**

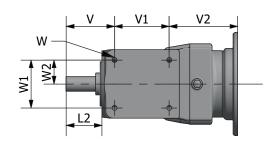


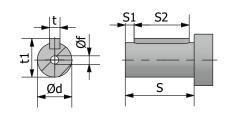




Gearbox	Motor	A	В	С	D	E	F	G	н	i	J	øк	L	М	N	Р	R	т	т1	Z
	IEC63 B5	184	186,5		11					8,5			232,5	115	95	140		4	12,8	
ED001	IEC71 B14a	185	187,5		14	00	47		149	C F	75	M6	233,5	85	70	105	٥٢	5	16,3	110
FRC01	IEC80 B14a	104	100 5	60	19	90	47	6,5	) 149	6,5	75	IVIO	000 5	100	80	120	8,5	6	21,8	110
	IEC90 B14a	184	186,5		24					8,5			232,5	115	95	140		8	27,3	
	IEC63 B5	195,5	198		11					8,5			254	115	95	140		4	12,8	
EDOGG	IEC71 B14a	196,5	199	70	14	100	F0	11.5	1.01	C F	٥٢	140	255	85	70	105	٥٢	5	16,3	110
FRC02	IEC80 B14a	1055	100	70	19	100	53	11,5	161	61 6,5	6,5 85	85	M8	100	80	120	8,5	6	21,8	118
	IEC90 B14a	195,5	198		24				8,5	5	254	115	95	140		8	27,3			

#### Foot & shaft





#### Foot

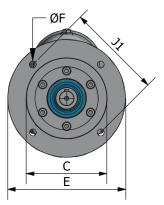
FUUL								
Gearbox	Motor	v	V1	V2	w	W1	W2	L2
	IEC63 B5			93				
FRC01	IEC71 B14a	C E E	74	94	M8	32,5	65	40 E
FRCUI	IEC80 B14a	65,5	14	02	IVIO	32,3	00	48,5
	IEC90 B14a		93					
	IEC63 B5			88				
FRC02	IEC71 B14a	91	75	89	M8	37,5	75	58,5
PhC02	IEC80 B14a	91	15	88	IVIÖ	31,5	15	56,5
	IEC90 B14a			00				

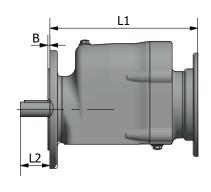
## Shaft

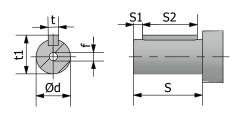
Silait								
Gearbox	Motor	d[h6]	Øf	s	S1	S2	t	t1
	IEC63 B5							
FRC01	IEC71 B14a	20	M8	40	5	32	6	22,5
FNCUI	IEC80 B14a	20	IVIO	40	3	32	0	22,0
	IEC90 B14a							
	IEC63 B5							
FRC02	IEC71 B14a	25	M10	50	3,5	40	8	28
111002	IEC80 B14a	20	IVITO	50	0,0	70	J	20
	IEC90 B14a							

Different solid shaft dimensions possible on request

#### Flanges

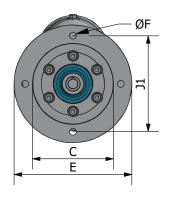


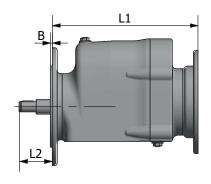




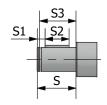
Gearbox	Flange	В	С	E	ØF	J1	Lı	L1 (IEC71)	L2	d[h6]	f	s	<b>S</b> 1	S2	t	t1
	SS 075 FL 120		80	120	6,6	100										
FRC01	SS 075 FL 140	3	95	140	a	115	200,5	201,5	40	20	M8	40	5	32	6	22,5
	SS 075 FL 160		110	160	9	130										
	SS 085 FL 140		95	140	0	115										
FRC02	SS 085 FL 160	4	110	160	9	130	130 211,5	212,5	50	25	25 M10	M10 50	3,5	40	8	28
	SS 085 FL 200		130	200	11	165										

#### B5T Flanges & Shafts









#### B5T output shaft

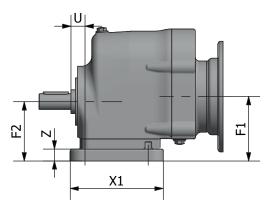
Gearbox	Shaft type	d[h6]	s	\$1	S2	S3	t	t1	L2
	SA12 B5T1	12	20,5			19,5	3	13,2	35
ED001	SA14 B5T1	1.4	00.5	4,5	14	01.1	_	150	32
FRC01	SA14 B5T2	14	22,5	,		21,1	3	15,2	41
	SA16 B5T3	16	26	6	18	24,1	4	17,5	51

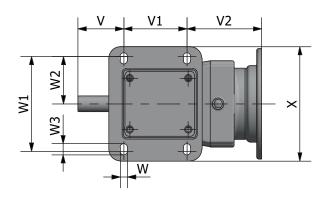
#### **B5T output flange**

Gearbox	Flange	Shaft	В	С	E	ØF	J1	Lı	L1 (IEC71)
	SS 075 FL 120 B5T1	SA12	3	80	120	6,6	100	200,5	201,5
FRC 01	SS 075 FL 160 B5T2	SA14 SA14	٥٢	110	160	9	130	107.5	100 5
	SS 085 FL 200 B5T3	SA16	2,5	130	200	13,5	165	197,5	198,5

# **General Dimensions**

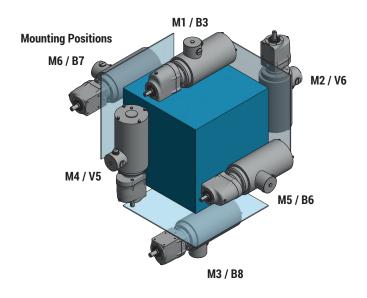
#### **Optional foot**



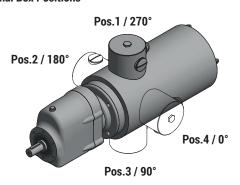


Gearbox	Foot	F2	U	v	V1	V2	V2 (IEC71)	w	W1	W2	W3	х	Х1	Z
ED001	M11	75	18	58	80	94,5	95,5	0	60	120	14	145	118	15
FRC01	G1	106	14	54	62	116,5	117,5	9	64	128	9	150	114	12
EDOOO	M21	80	10	60	87	99	100	9	55	110	14	145	125,5	15
FRC02	G2	125	18	68	72	114	115	11	80	160	11	185	126	16

#### **Extra information**



#### **Terminal Box Positions**



#### **Lubrication Quantity**

Oil Quantity in ML.	Mounting Position								
Gearbox	M1 (B3)	M3 (B8)	M6 (B7)	M5 (B6)	M4 (V5)	M2 (V6)			
FRC 01	600	450	250	250	400	400			
FRC 02	*	*	*	*	*	*			

<sup>\*</sup> in development

#### **Lubrication Type**

_ubiloution iyp		
Lubrication Brand	Lubrication Type	
Matrix	Foodmax 460	Standard
Castrol	Optileb GT 460	Alternative
Bechem	Berusynth 460H1	Alternative
Shell	Casida Fluid GL460	Alternative
Mobil	SHC Cibus 460	Alternative

#### **Debreather Positions**

M1 / B3	M3 / B8	M5 / B6
M6 / B7	M4 / V5	M2 / V6

#### Weight

Gearbox	Weight
FRC 01	9.0 Kg
FRC 02	*

\* in development

Given values are an average and may vary depending on oil quantity.

# **General Dimensions**



#### Dertec

Einsteinpark 1 2171 TX Sassenheim The Netherlands

**T** +31 71 409 2 409 **E** info@dertec.com

FRC Documentation - 1.0 3/3/2022

www.dertec.com

